

Connection of load cells



Welcome to the webinar: “Connection of load cells”

A graphic featuring the word "WEBINAR" in a blue, sans-serif font. The "W" is contained within a dark blue circle, and the entire graphic is set against a light gray rounded rectangle with a subtle reflection below it.

WEBINAR

Thomas Kleckers

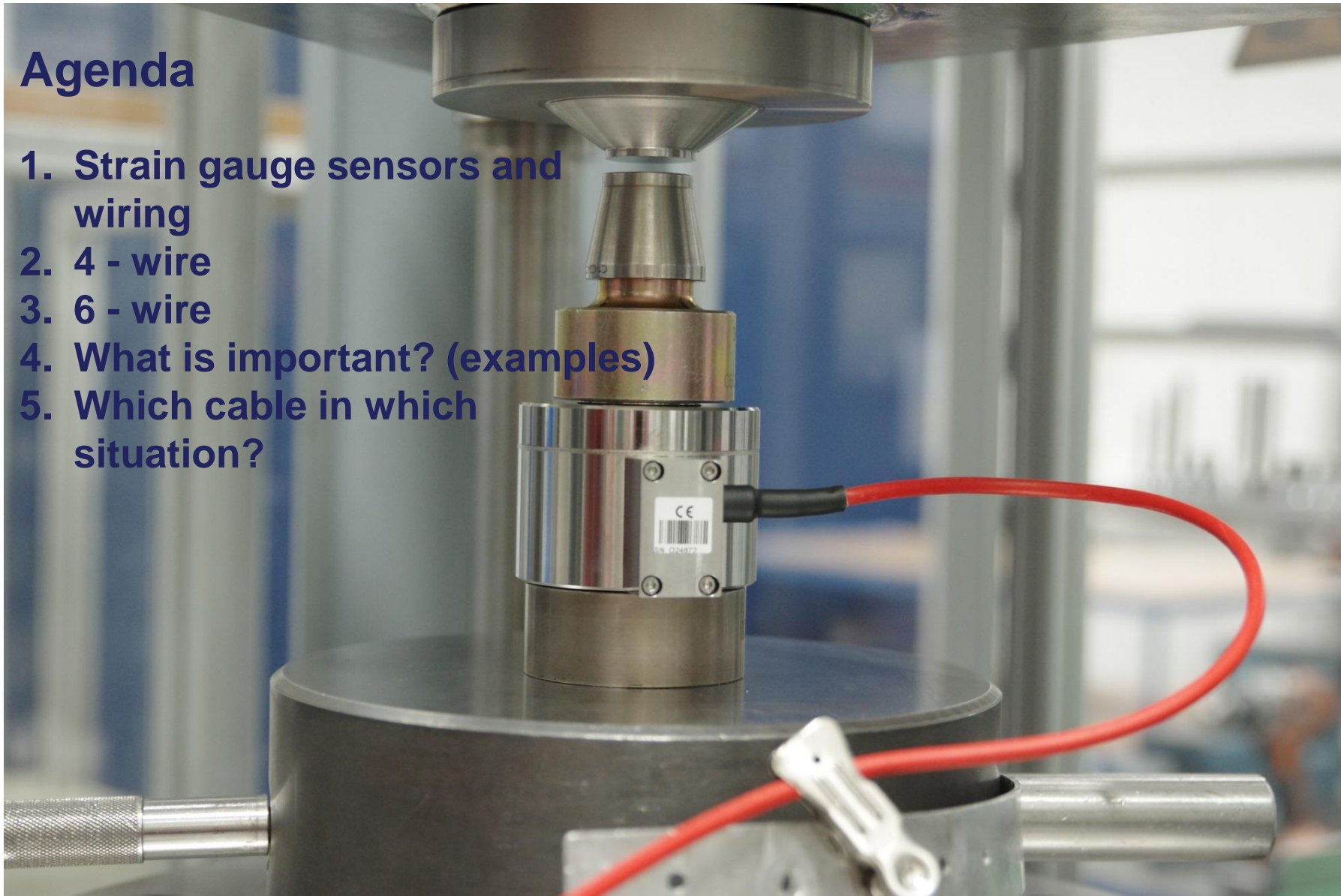
- **Product Manager Force Transducers**
- Diploma Physical Engineering
- 16 years of experience in development (strain gauges), 10 years responsibility for force sensors at HBM
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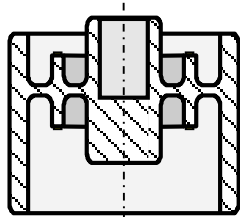
Thomas Kleckers

Agenda

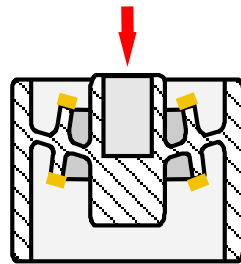
1. Strain gauge sensors and wiring
2. 4 - wire
3. 6 - wire
4. What is important? (examples)
5. Which cable in which situation?



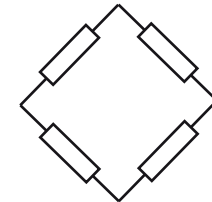
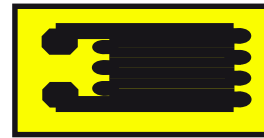
Strain gauge sensors: The principle



Spring body



If a load is introduced, strain appears. Strain gauges convert the strain into a change of resistance



The Wheatstone bridge converts the changes in resistance into a measurable voltage

Typical:

Mech. Stress:	2	200 Mpa
Material:		Steel (200 Gpa)
Strain $\epsilon = \sigma/E \Rightarrow$		0,001 (= 0,1 %)
Usual "Unit":		$\mu\text{m}/\text{m} = 10^{-6}$



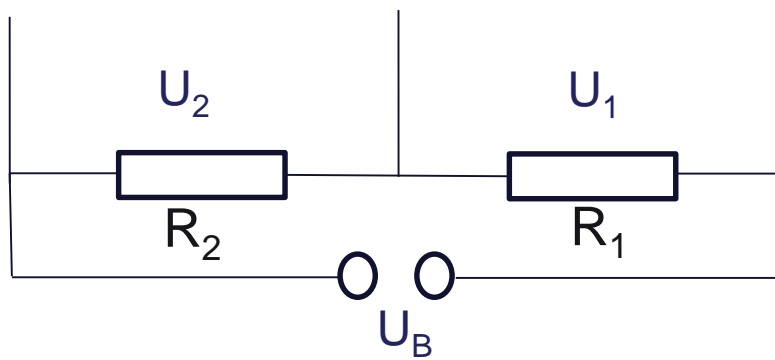
How much is the change in resistance?

$$\Delta R/R_0 = k \cdot \varepsilon \quad k \sim 2 \quad R_{(\text{typ.})} = 350\Omega$$

$$\varepsilon = 1000 \mu\text{m/m} (0,1 \%)$$

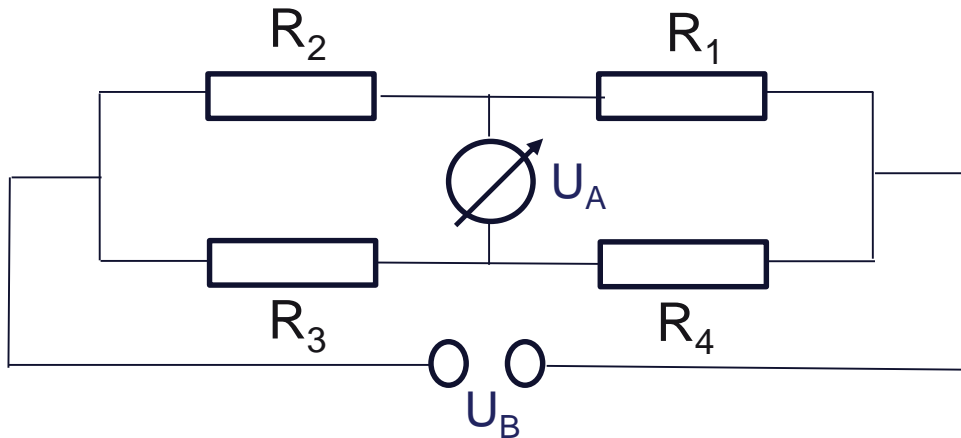
Strain gauge resistance 350 Ohm Strain 1000 $\mu\text{m/m}$:
0,7 Ω change of resistance

Ohmmeter: Resolution by far not good enough!
=> Wheatstone Bridge



$$U_1 = \frac{R_1}{R_1 + R_2} * U_B$$

$$\frac{U_1}{U_B} = \frac{R_1}{R_1 + R_2}$$



$$\frac{U_A}{U_B} = \frac{R_1}{R_1 + R_2} - \frac{R_4}{R_3 + R_4}$$

Simplification: $R_1 = R_2$ and $R_3 = R_4$

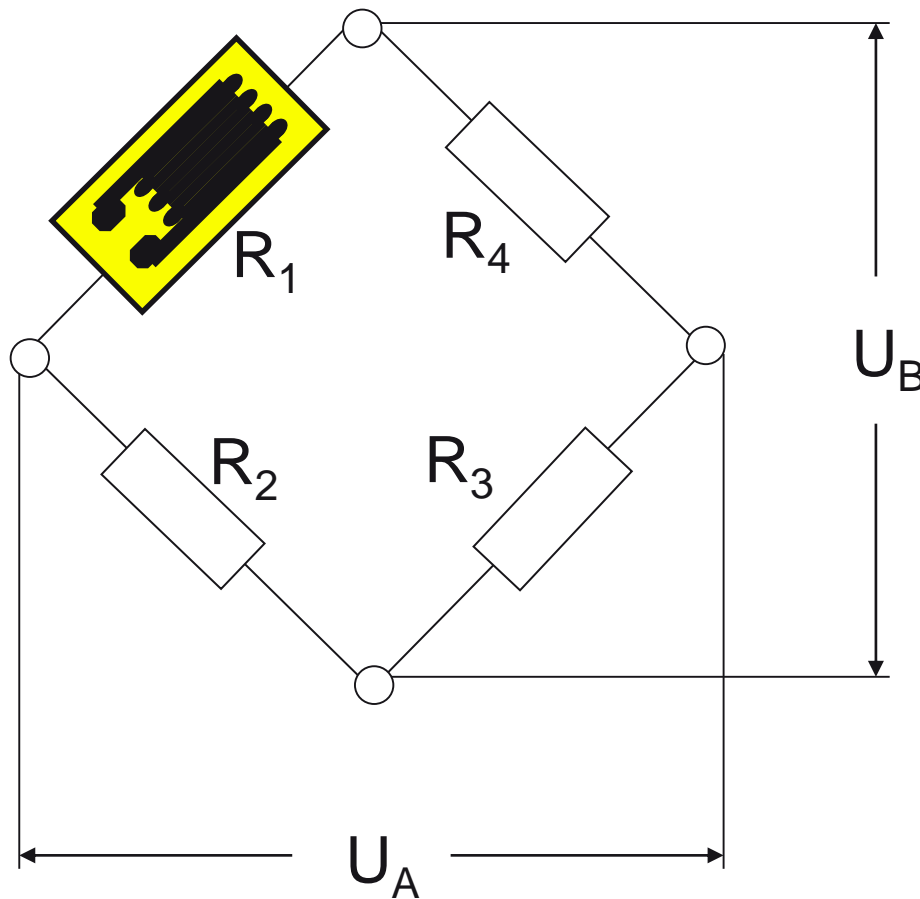
$$\frac{U_A}{U_B} = \frac{1}{4} \cdot \left(\frac{\Delta R_1}{R_1} - \frac{\Delta R_2}{R_2} + \frac{\Delta R_3}{R_3} - \frac{\Delta R_4}{R_4} \right)$$

R_1, R_3 : **Increase** of resistance lead to a positive output voltage

R_1, R_2 : **Decrease** of resistance lead to a positive output voltage

Example:

1000 $\mu\text{m}/\text{m}$, change in resistance 0.7 Ohm



$$\frac{U_A}{U_B} = \frac{R_1}{R_1 + R_2} - \frac{R_4}{R_3 + R_4}$$

$$\frac{U_A}{U_B} = \frac{1}{4} \cdot \left(\frac{\Delta R_1}{R_1} - \frac{\Delta R_2}{R_2} + \frac{\Delta R_3}{R_3} - \frac{\Delta R_4}{R_4} \right)$$

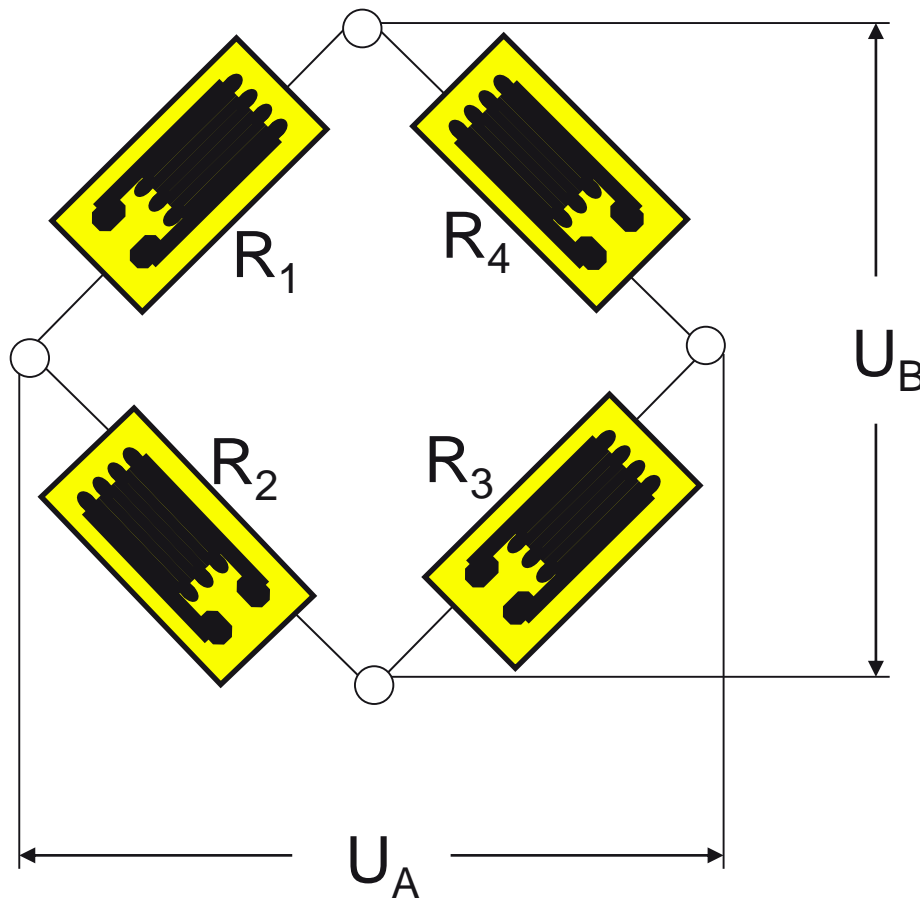
$$\frac{U_A}{U_B} = \frac{1}{4} \cdot \left(\frac{0.7 \Omega}{350 \Omega} - \frac{0 \Omega}{350 \Omega} + \frac{0 \Omega}{350 \Omega} - \frac{0 \Omega}{350 \Omega} \right)$$

$$\frac{U_A}{U_B} = 0,0005$$

$$\frac{U_A}{U_B} = 0,5 \text{ mV/V}$$

Example:

1000 $\mu\text{m}/\text{m}$, change in resistance 0.7 Ohm



$$\frac{U_A}{U_B} = \frac{R_1}{R_1 + R_2} - \frac{R_4}{R_3 + R_4}$$

$$\frac{U_A}{U_B} = \frac{1}{4} \cdot \left(\frac{\Delta R_1}{R_1} - \frac{\Delta R_2}{R_2} + \frac{\Delta R_3}{R_3} - \frac{\Delta R_4}{R_4} \right)$$

$$\frac{U_A}{U_B} = \frac{1}{4} \cdot \left(\frac{0,7 \Omega}{350 \Omega} - \frac{-0,7 \Omega}{350 \Omega} + \frac{0,7 \Omega}{350 \Omega} - \frac{-0,70 \Omega}{350 \Omega} \right)$$

$$\frac{U_A}{U_B} = 0,002$$

$$\frac{U_A}{U_B} = 2 \text{ mV/V}$$

$$\frac{U_A}{U_B} = 2 \text{ mV/V}$$

Common supply voltages (U_B):

Between 1 V and 10 V
Very common: **5 V**

Output voltage with full scale:

$$U_{A(fs)} = 2 \frac{\text{mV}}{\text{V}} * 5 \text{ V}$$

$$U_{A(fs)} = 10 \text{ mV}$$



Resolution: 10000 digits:

1 μ V

- Rated output of the load cell: 2mV/V
- Supply voltage: 5V
- Max. output voltage: 10mV
- Resolution 100000d: 0,1 μ V

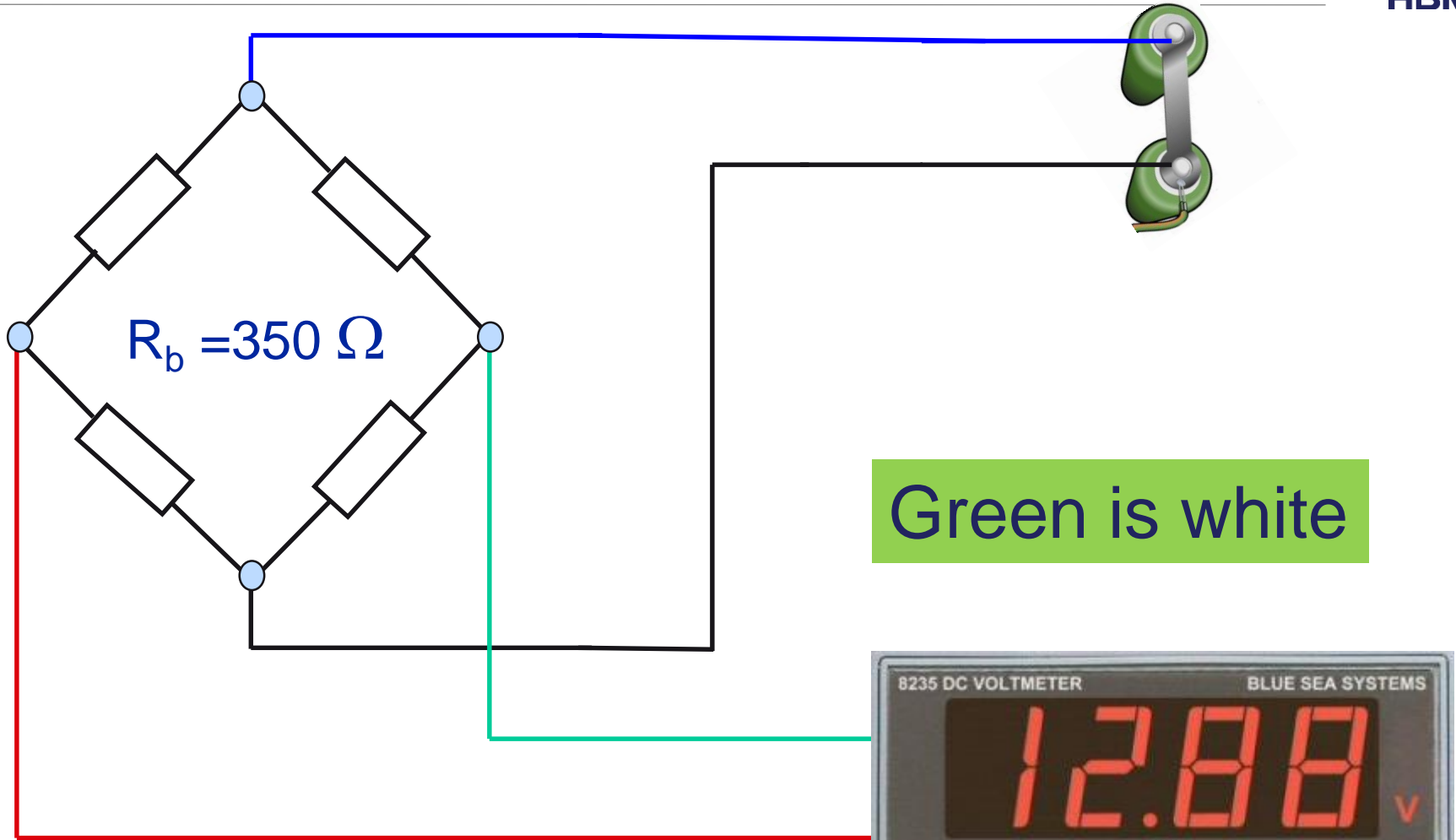
- Comparisson:
- 321 m
- 3,21 mm Thickness of a CD jewel case

Influences

- *Electrical fields (50 Hz, inverter)*
- *Magnetic fields changing with the time*



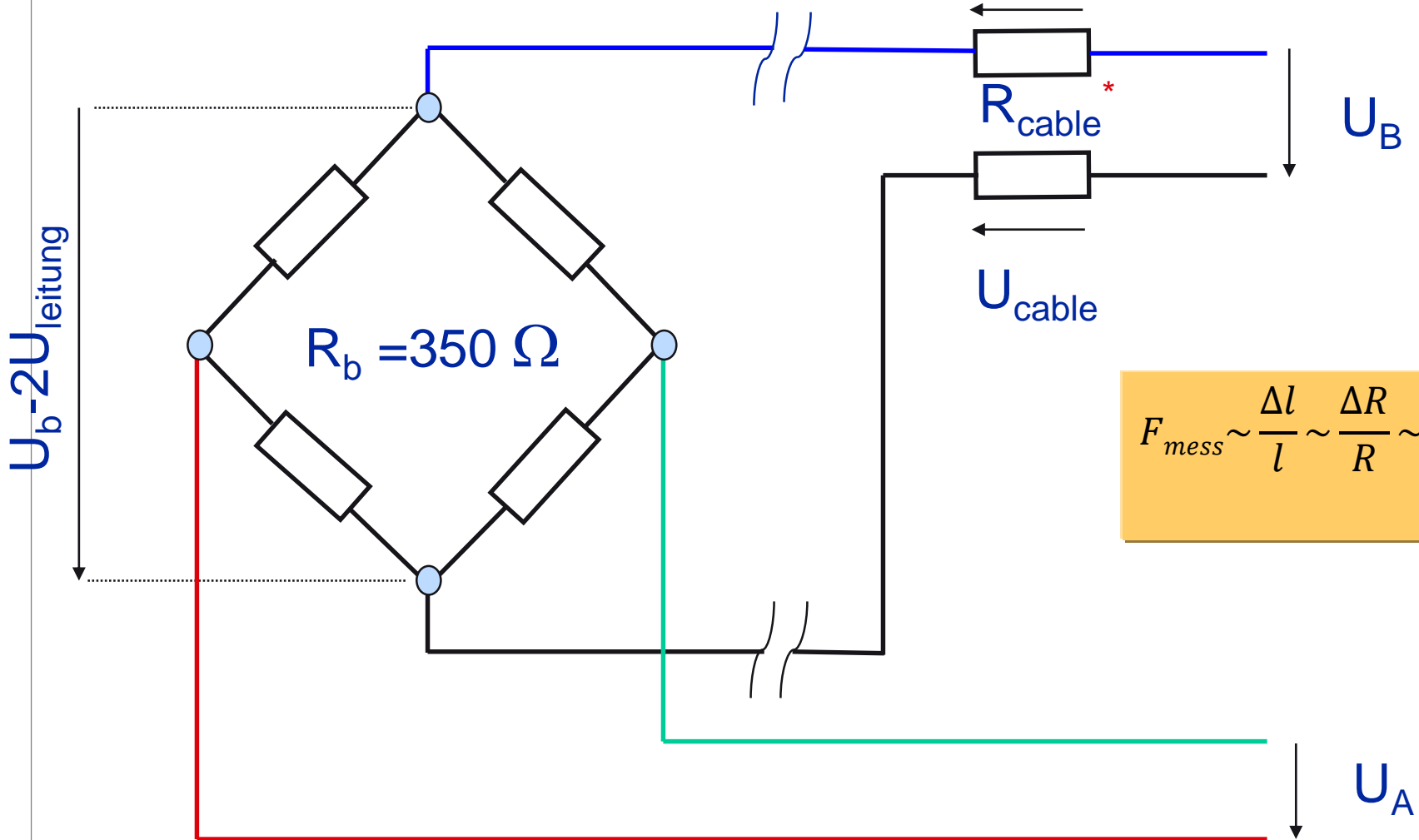
4 – wire circuit



$$\frac{U_A}{U_B} = \frac{k}{4} (\epsilon_1 - \epsilon_2 + \epsilon_3 - \epsilon_4)$$



4 – wire circuit



$$F_{mess} \sim \frac{\Delta l}{l} \sim \frac{\Delta R}{R} \sim \frac{U_A}{U_B}$$

No influence of the resistance of the output wires on the results due to high input resistance of amplifier

Example

- Bridge Resistance: 350 Ω
- Copper wire, 0,14 mm²
- spec. Resistance $\rho=17,8 \Omega \cdot \text{mm}^2/\text{m}$

$$R_{\text{wire}} = \frac{\rho l}{A}$$

Case 1: 5 m Cable length:

- $2 \cdot R_{\text{wire}} = 1,272 \Omega$
- Sensitivity change: 0,36 %

Fall 1: 50 m Cable length :

- $2 \cdot R_{\text{wire}} = 1,272 \Omega$
- Sensitivity change: 3,6 %

Conclusion

- Perform calibration with the cable used in the measurement
=> HBM is doing so
- Cable extension may be critical: Shunt calibration?
- *Best thing is to do cable extension by using the 6 wire technology*



Cable resistance is depending on temperature



Higher temperature



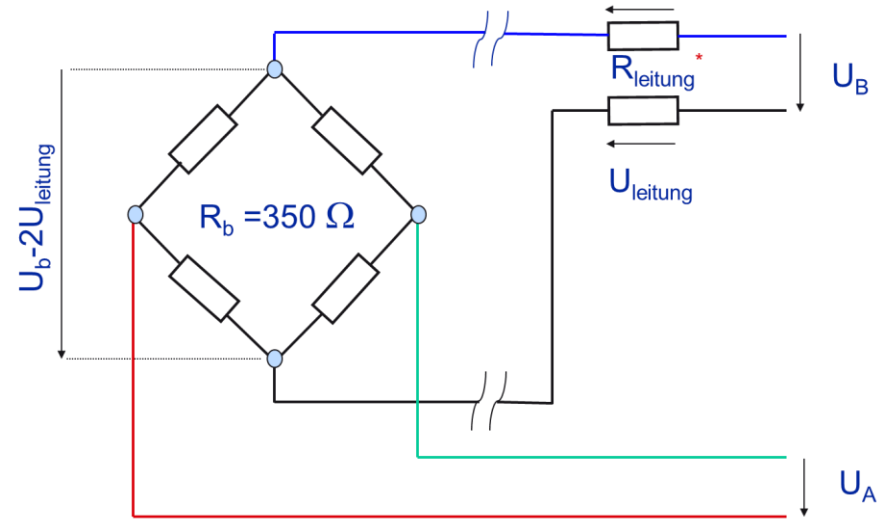
Higher cable resistance



Lower voltage at the Wheatstone bridge



Lower sensitivity

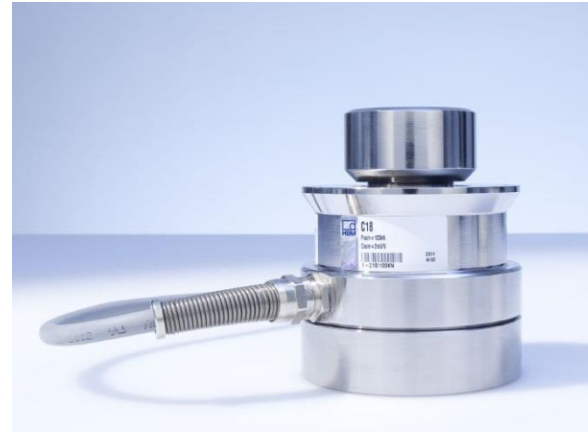


Sensitivity is depending on cable length and temperature (only for 4 – wire!)



With HBM: All characteristics include the cable delivered with the sensor.

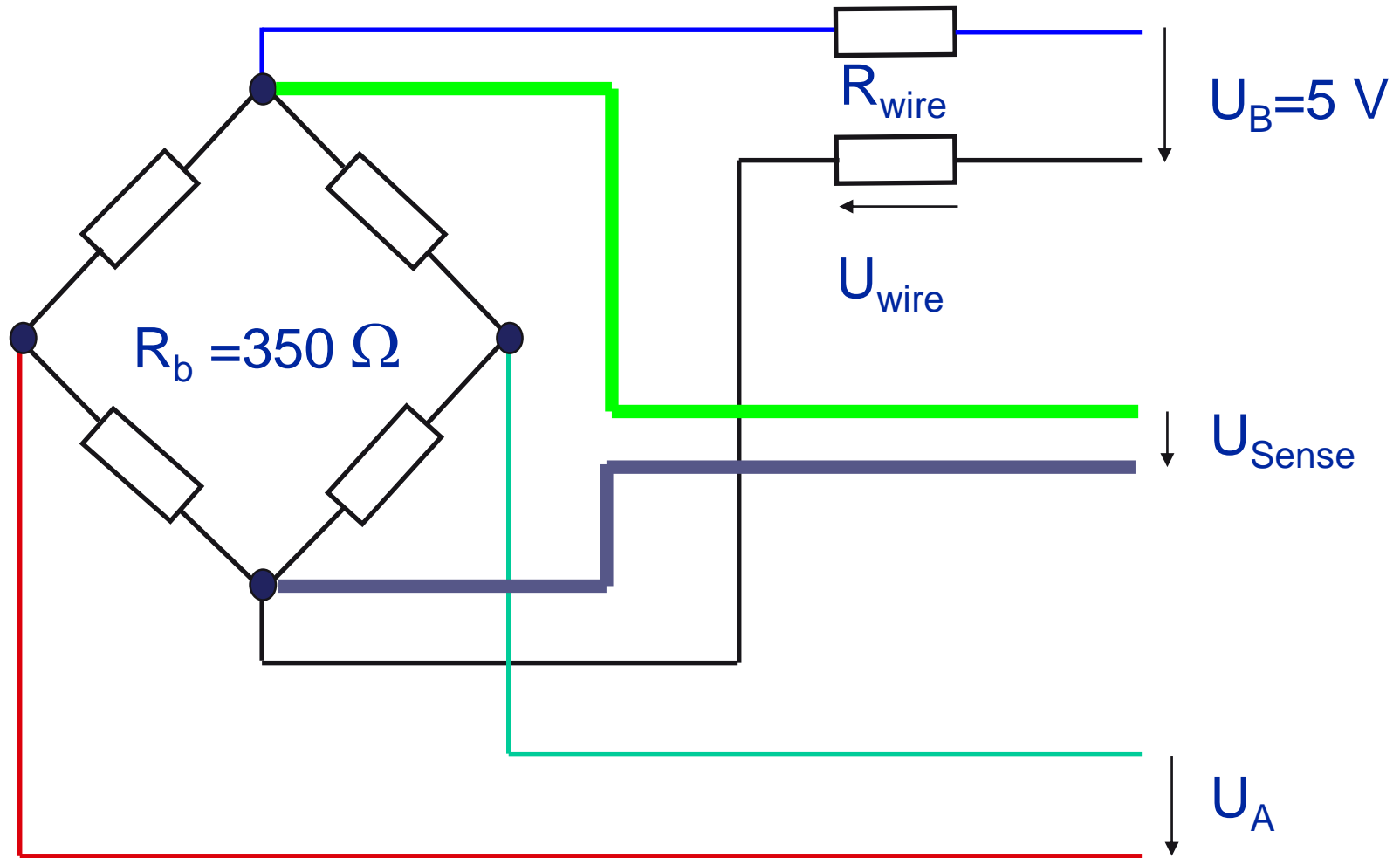
4 – wire circuit



Load cells with 4 – wire connection



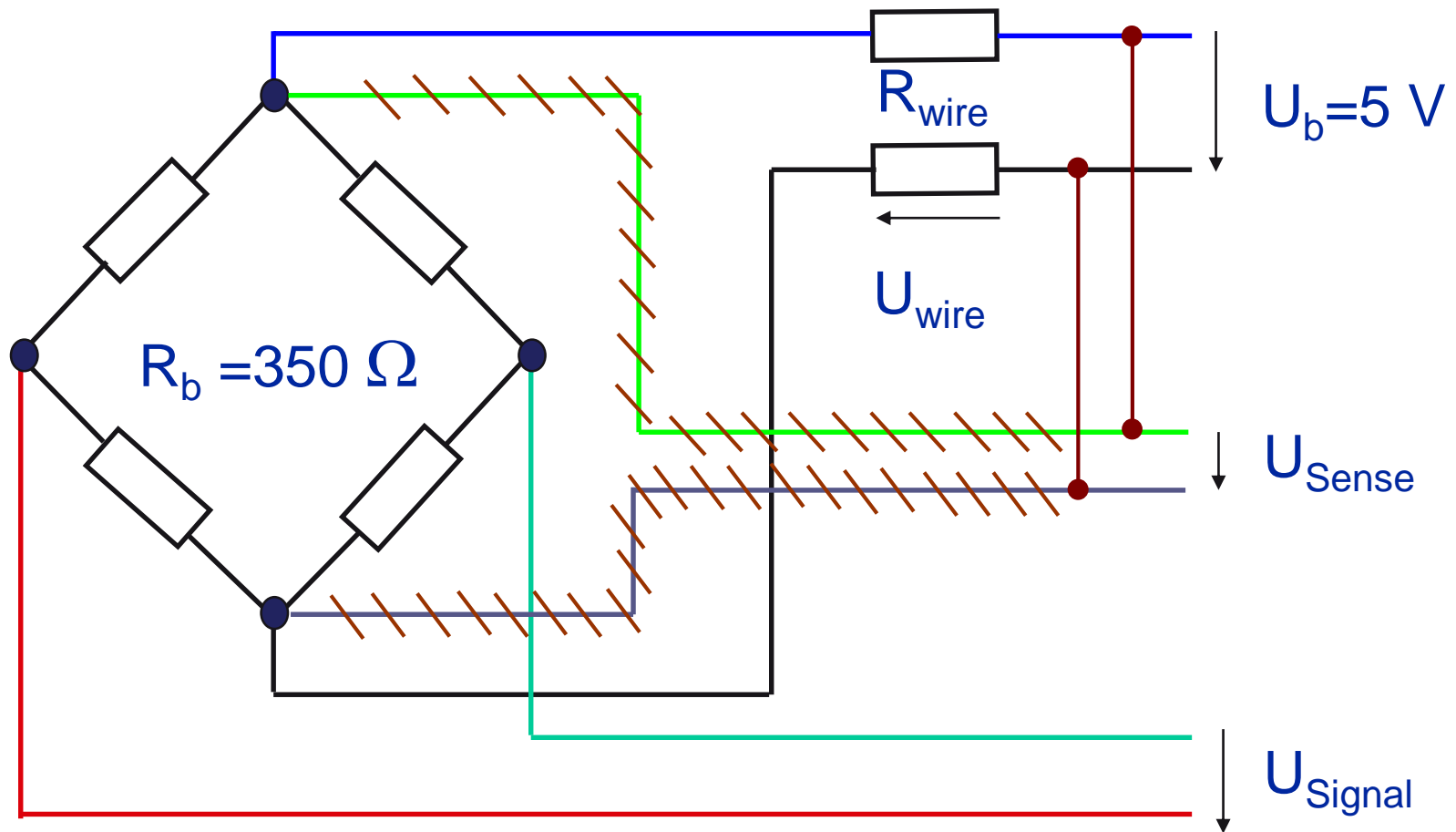
Sensors have to be calibrated in mounting position in 4 – wire connection



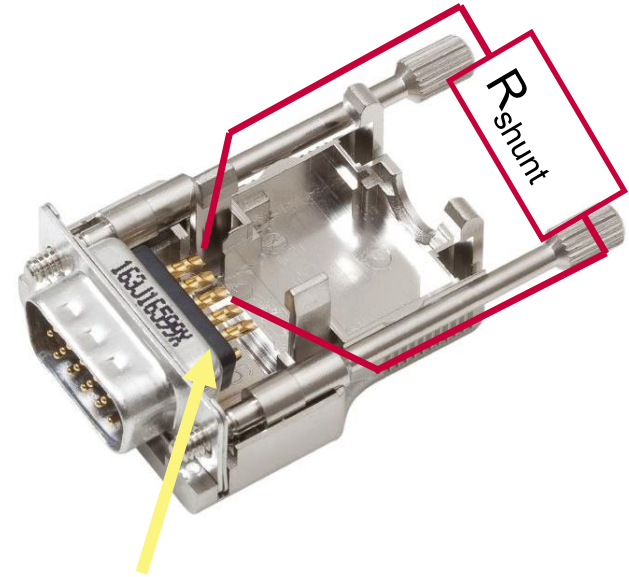
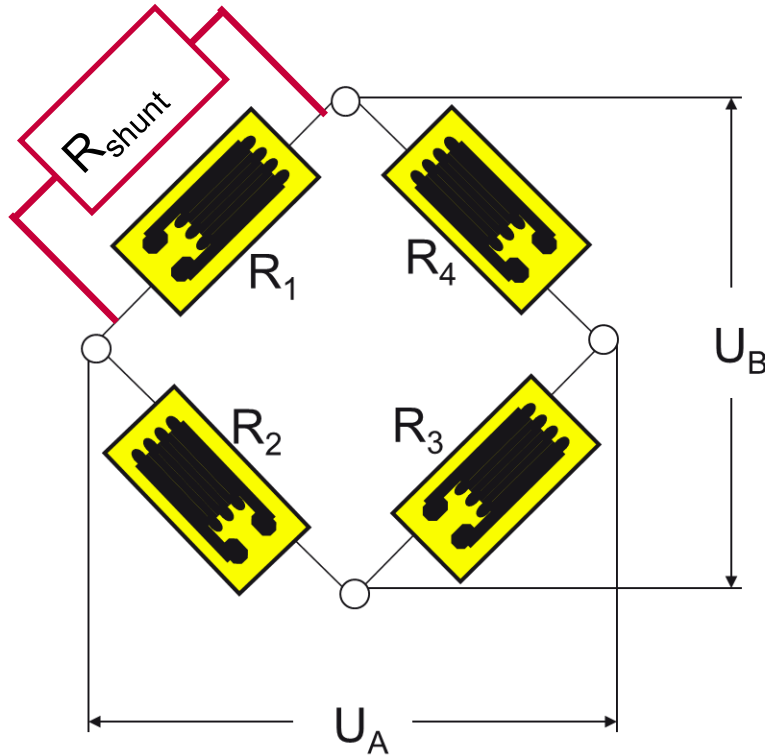
6 – wire circuit: Measurement of the voltage at the Wheatstone bridge, readjustment if required, for example in case of changes in temperature

6 – wire circuit

=> No connection between sense wires and bridge supply, e.g. in the connector



What is important? (examples)



Remove flux!

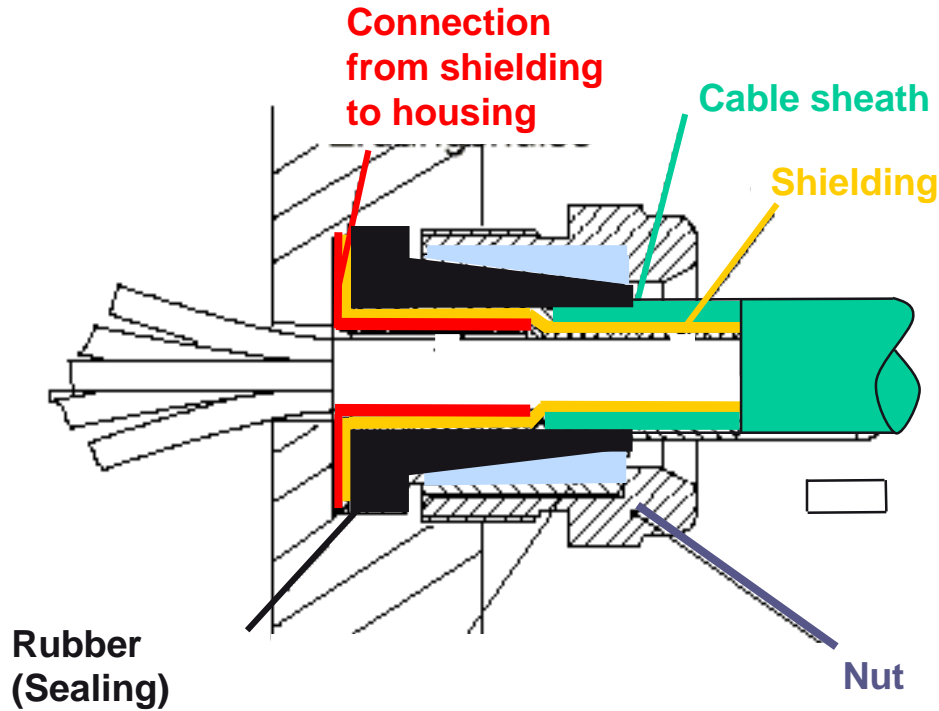
$$\frac{\Delta R}{R} = \frac{R_1 - \frac{R_1 + R_{Shunt}}{R_1 \times R_{Shunt}}}{R_1}$$

Flux changes ist resistance if humidity appears.

=> String influence on zero point

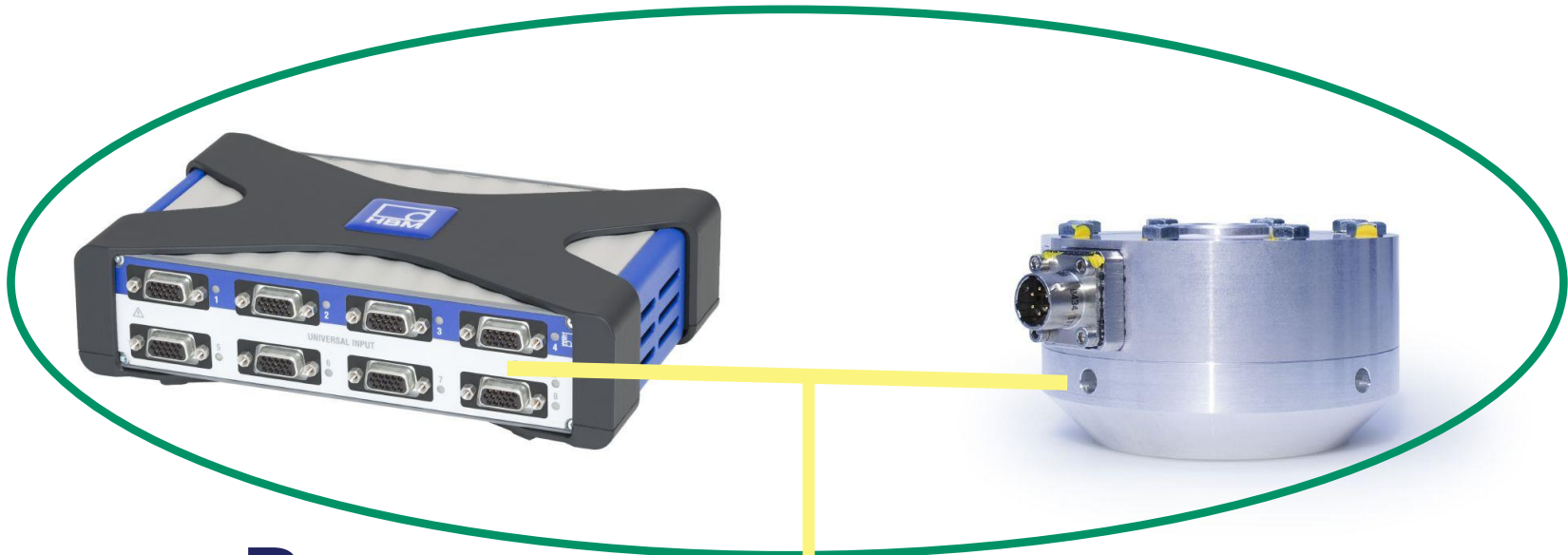
$$\frac{U_A}{U_B} = \frac{1}{4} \cdot \left(\frac{\Delta R_1}{R_1} - \frac{\Delta R_2}{R_2} + \frac{\Delta R_3}{R_3} - \frac{\Delta R_4}{R_4} \right)$$

- Cable shielding is connected to sensor housing



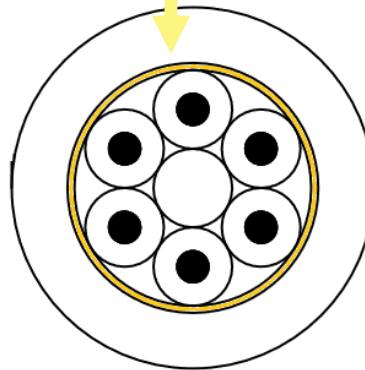
⇒ Faraday's cage ⇒ good EMC protection ⇒ test condition at HBM

What is important? (examples)



P_1

P_2



$P_1 \neq P_2 \rightarrow I$



Problem of the concept using the Faraday's cage:

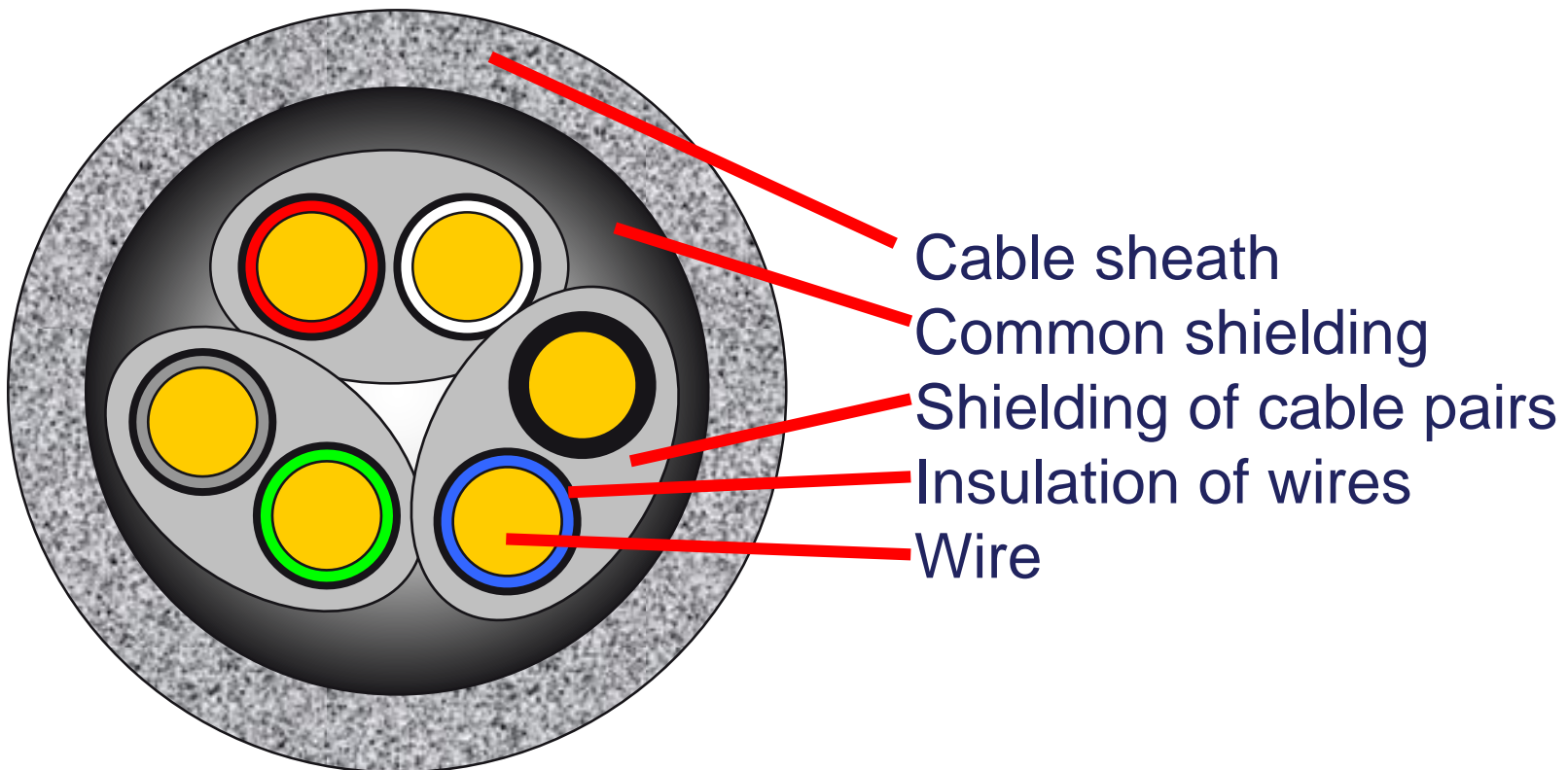
- If the sensor and the amplifier are not on the same electrical potential
=> Current flows over the shielding
- 50 Hz – interferences may occur

Solution:

- Use a low resistance connection between sensor and amplifier housing
- Recommendation: very flexible wire, 16 mm² Cu

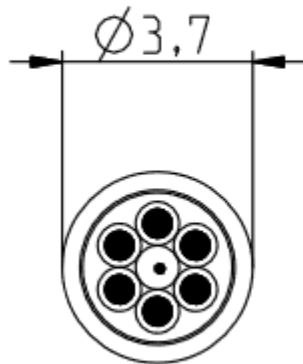
Which cable?

- Number of wires (4 L or 6 L?)
- Cross section (Cable length)
- Temperature
- Withstanding against chemicals
- Mechanical requirements (drag chain?)



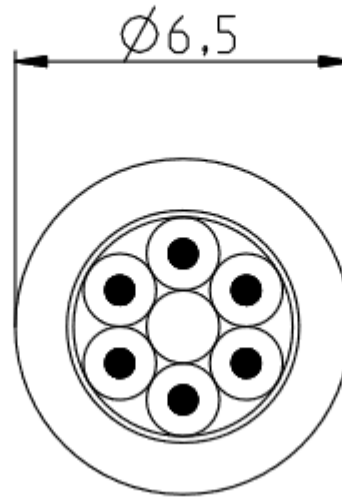
Which cable?

KAB131



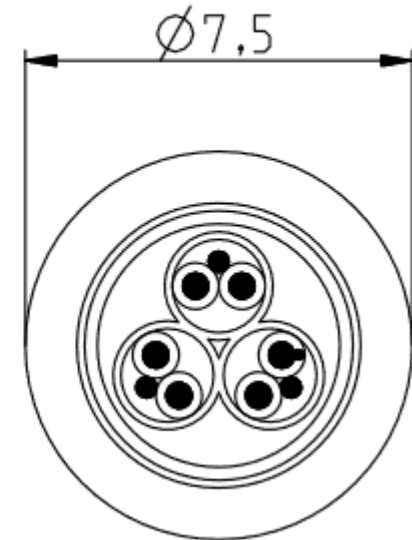
- Very flexible
- Low force shunt
- Withstands many operating materials
- Higher electrical resistance
- Higher capacity

KAB157



- Withstands many operating materials
- High symmetry
- For outdoor use

KAB139B

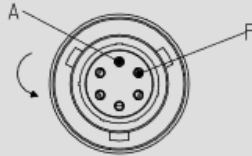


- Double shielding concept, low capacity works with long distances, high CF and under harsh EMC - environment
- Stiff

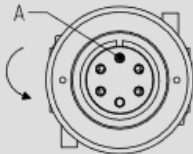
Which cable?

Male connector on sensor-side

B, L = bayonet



G = thread

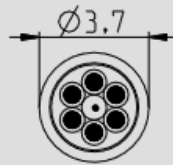


Z = 7-pin binder

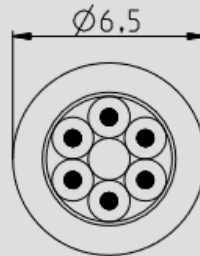


Cable types

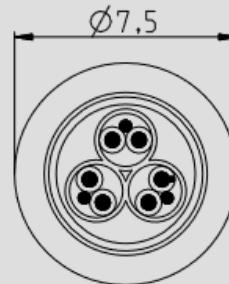
KAB-131



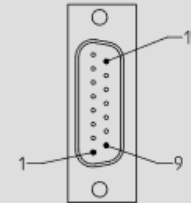
KAB-157



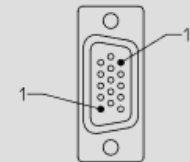
KAB-139B



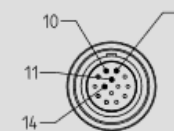
Connection variants for the amplifier



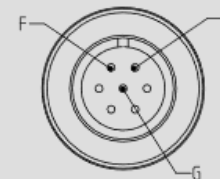
F = Sub-D



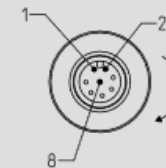
Q = Sub-HD



QP = 14-pin ODU



N = Greenline



M = 8-pin,
M12 female connector

K-CAB-F