

Dynamic Power Measurement and Accelerated Efficiency Mapping

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HBK – Who we are



Complementary discipline expertise

Sound, noise and vibration



Reliability, durability, propulsion efficiency, electrical properties, weighing

Complementary domain expertise

Frequency domain



Time domain

Combined covering the complete measurement chain

Sensors | Data acquisition | Data preparation | Data evaluation | Engineering

As the product physics experts

We deliver valuable insights through three physical domains

MECHANICAL



SUB-DOMAINS

- Strain
- Load
- Torque
- Force
- Pressure
- Durability

EXAMPLES OF OUR TASKS

- Weighing bottles on a production line to ensure the correct amount
- Measuring the torque generated by an electric motor driving a hybrid vehicle
- Measuring the strain in an aircraft wing as it is tested for durability and ultimate load

SOUND & VIBRATION



SUB-DOMAINS

- Noise
- Sound quality
- Sound power
- Acoustics

Designing optimal car sound quality – inside/outside
Evaluating acoustics in new buildings
Improving cabin comfort in passenger aircraft
Ensuring mobile phone production sound quality
Vibration testing satellites before launching into space

ELECTRICAL



SUB-DOMAINS

- Electrical signals
- Voltage
- Current
- Speed
- Temperature

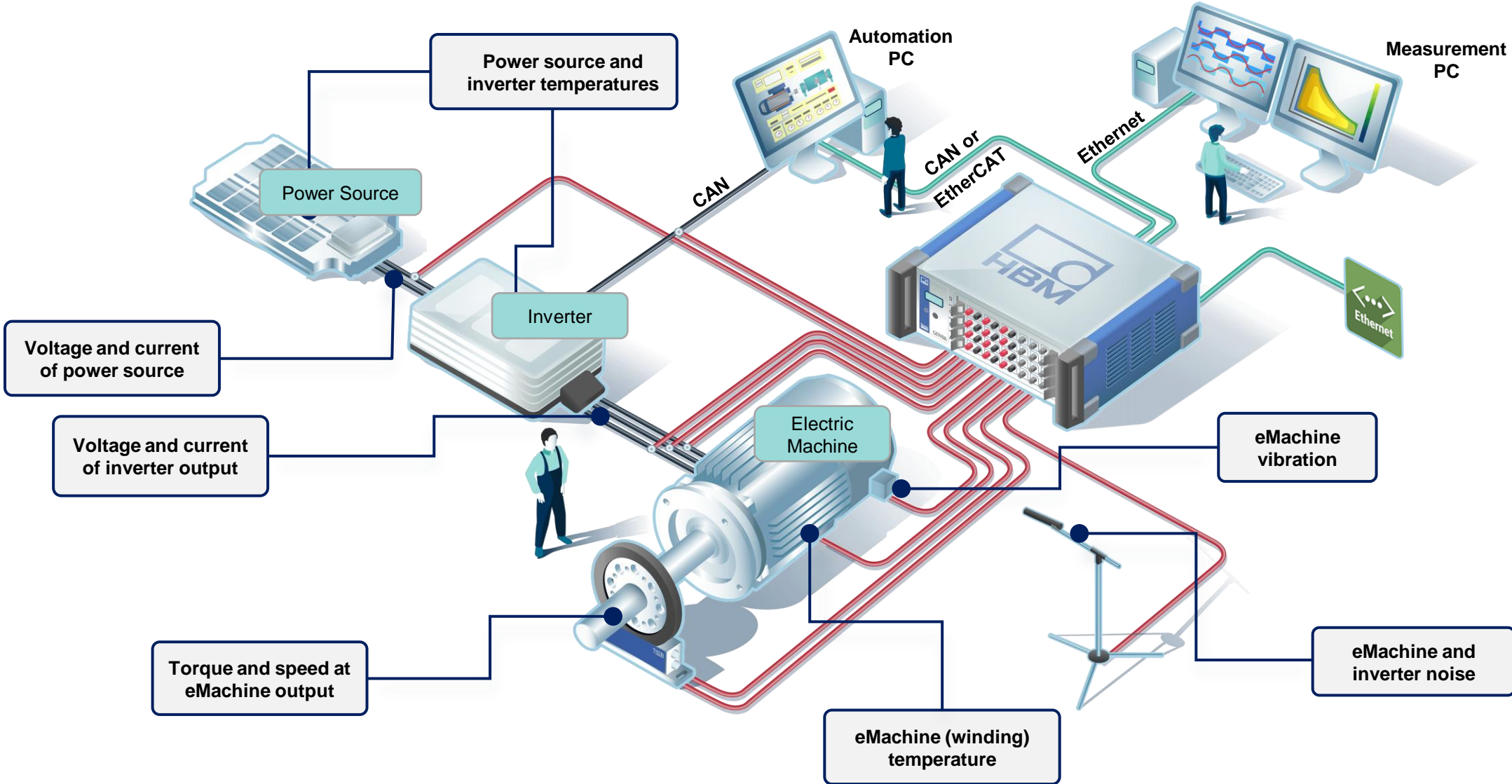
EXAMPLES OF OUR TASKS

- Testing inverters powering electric vehicles
- Checking the reliability of power grids
- Optimising performance and range of electric vehicle motors

Agenda

1. Electric power train
2. Conventional electric power calculation
3. Dynamic electric power approximation
4. Comparative measurements
5. Accelerated efficiency mapping
6. Conclusion

Electric Power Train

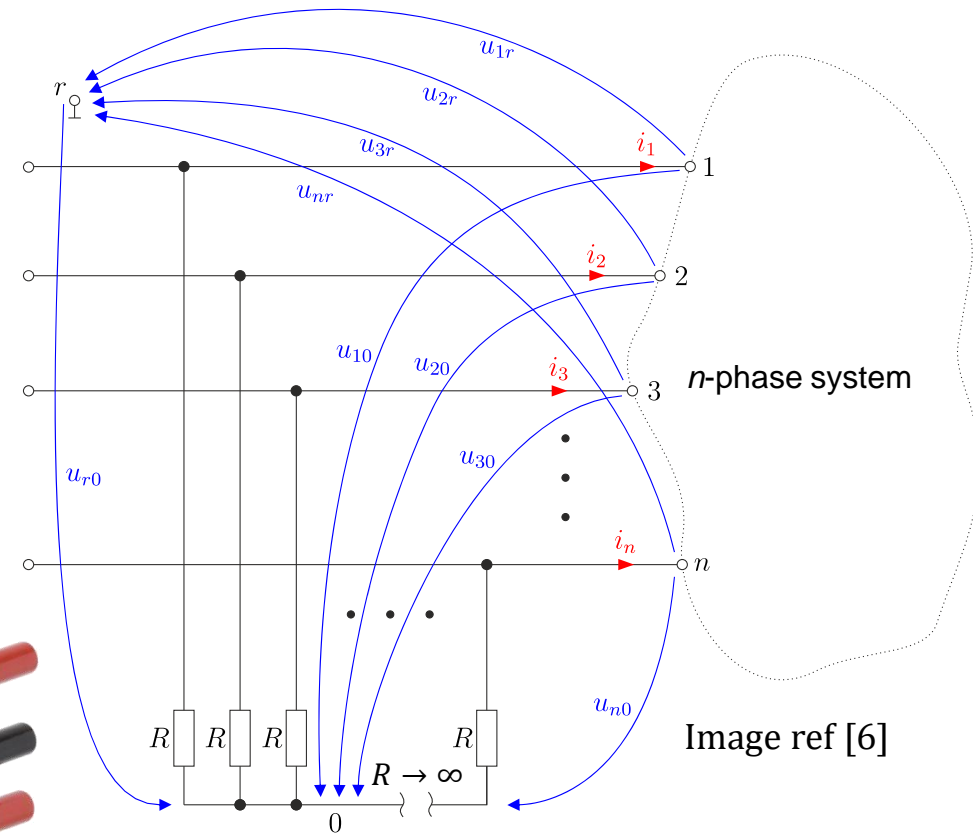


How to Measure Voltages and Currents

Recommendation for Power analysis [5,6]

- ▲ Voltages may be measured
 - against any arbitrary common reference potential r
 - Phase to phase with different reference phases
- ▲ Calculate phase to natural zero voltages $u_{v0}(t)$ before analyzing power quantities
- ▲ Measure the line currents
- ▲ Zero-sum quantities for power analysis

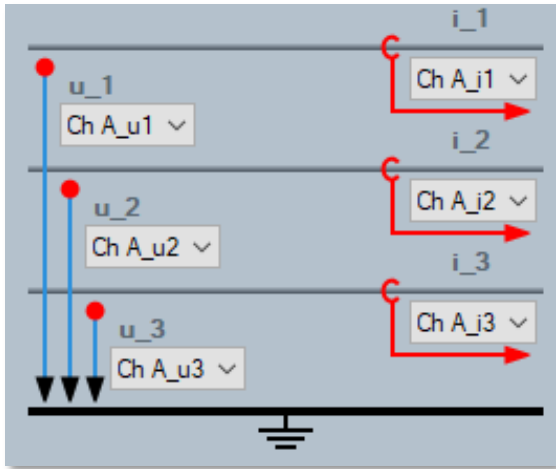
$$\sum_{v=1}^n i_v(t) = 0 \qquad \sum_{v=1}^n u_{v0}(t) = 0$$



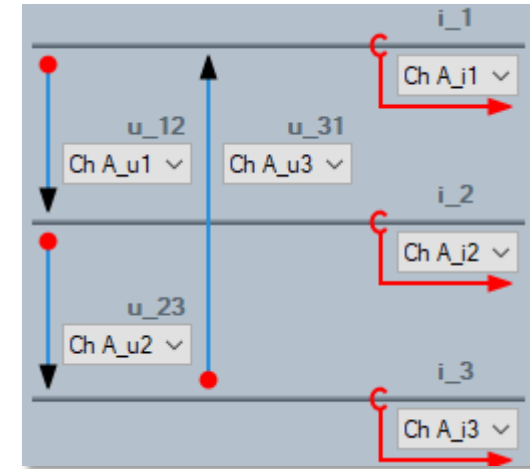
How to Measure Voltages and Currents

Phase to ground /

Phase to common arbitrary reference potential



Phase to phase



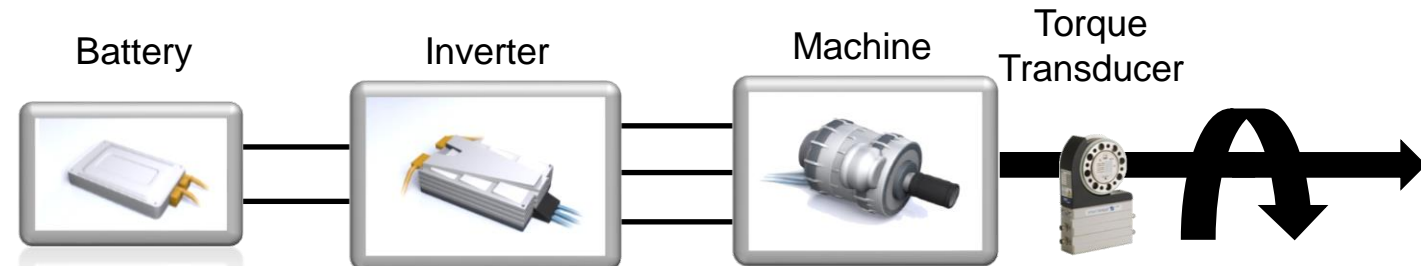
Inverter.out.u_1	$((2 * RTFomulas.Inverter.out.u_{1G}) - RTFomulas.Inverter.out.u_{2G} - RTFomulas.Inverter.out.u_{3G}) / 3$
Inverter.out.u_2	$((2 * RTFomulas.Inverter.out.u_{2G}) - RTFomulas.Inverter.out.u_{3G} - RTFomulas.Inverter.out.u_{1G}) / 3$
Inverter.out.u_3	$((2 * RTFomulas.Inverter.out.u_{3G}) - RTFomulas.Inverter.out.u_{1G} - RTFomulas.Inverter.out.u_{2G}) / 3$

Inverter.out.u_1	$(RTFomulas.Inverter.out.u_{12} - RTFomulas.Inverter.out.u_{31}) / 3$
Inverter.out.u_2	$(RTFomulas.Inverter.out.u_{23} - RTFomulas.Inverter.out.u_{12}) / 3$
Inverter.out.u_3	$(RTFomulas.Inverter.out.u_{31} - RTFomulas.Inverter.out.u_{23}) / 3$

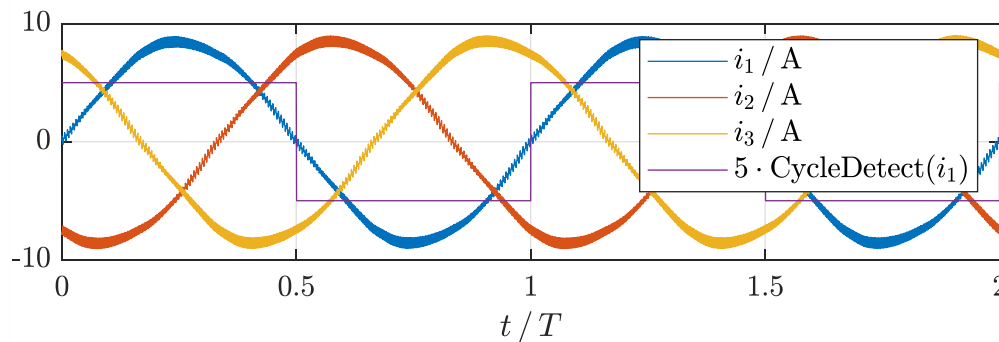
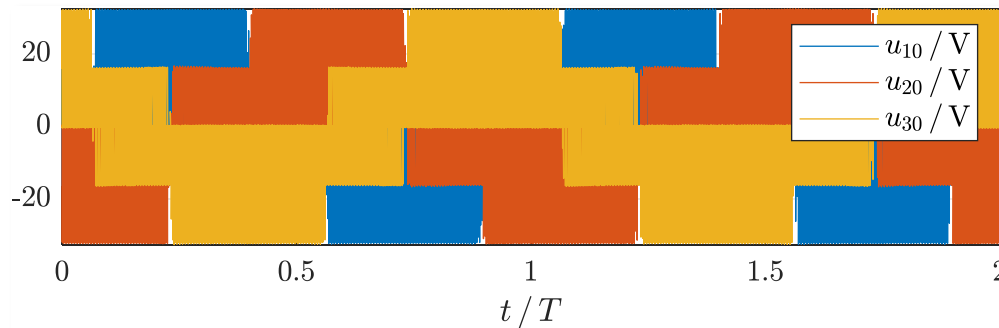
Conventional Electric Power Calculation

Input power of the machine

1. Measurement of the line currents and voltages
2. Detection of the fundamental cycle (based on smooth current waveform)



u_{10}, u_{20}, u_{30} (blue arrows)
 i_1, i_2, i_3 (red arrows)



Cycle is the basis of all calculations related to the fundamental period, such as:

RMS values, active, reactive and apparent power

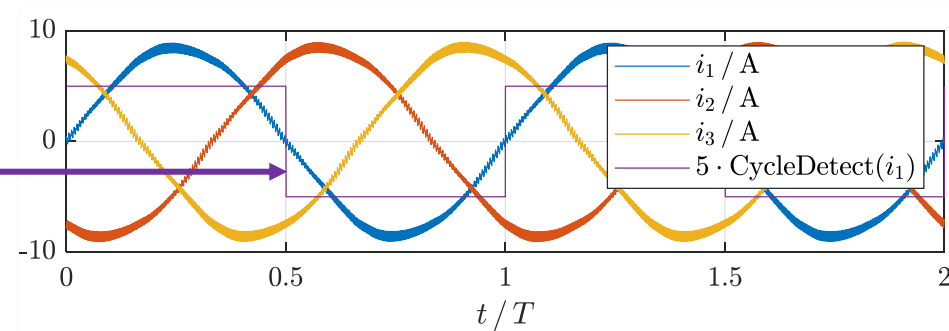
Conventional Electric Power Calculation

- ▲ Calculation of the **instantaneous power** [1-6]

$$p(t) = u_{10}(t) \cdot i_1(t) + u_{20}(t) \cdot i_2(t) + \dots + u_{n0}(t) \cdot i_n(t)$$

- ▲ Calculation of the **active power** as the **average** of the instantaneous power related to the **fundamental period** T [1-6] → fundamental period is defined by the previously determined cycle

$$P = \overline{p(t)} \Big|_T = \frac{1}{T} \cdot \int_T p(\tau) d\tau$$



- ▲ Further cycle-based parameters, such as power quantities, RMS values, fundamentals, etc., may be implemented analogously

Configuration of the ePower Suite

The screenshot displays the ePower Suite software interface, configured for a power source, inverter, and motor system. The interface is divided into several sections:

- Left Panel (Control and Settings):** Includes fields for 'Next experiment name' (Recording 012), 'Acquisition' settings (Sample rate: 2 MS/s), and 'Acquisition Control' (Preview, Record, Stop, Trigger). It also has 'Settings' (Generic, Optional Analysis) and 'Functionality' (Create Results, Create Mapping, Zero/Shunt, Copy, Review Formulas, Freeze) buttons.
- System Overview (Top):** Shows a block diagram with three main components:
 - Powersource:** DC input, output current i_{mean} 4,91 A, output voltage u_{mean} 48,15 V, output power P 236,42 W, Frequency 74,97 Hz. Currents: 10,89 A; Voltages: 1 kV.
 - Inverter:** Collective output, output current i_L 9,03 A, output voltage u_U 14,69 V, output power P 226,18 W, Frequency 74,96 Hz. Currents: 33,77 A; Voltages: 100 V.
 - Motor:** Collective output, output torque M 1,12 Nm, output speed n 1499,3 RPM, output mechanical power P_{mech} 175,26 Nm/s, Frequency 74,97 Hz. Torque: 1,000 kNm; Speed: 1000 RPM.
- Efficiency Calculations (Bottom Middle):**
 - Inverter_Eff:** P_{in} 236,42 W, P_{out} 226,11 W, η 95,64%, P_{loss} 10,32 W.
 - Motor_Eff:** P_{in} 226,18 W, P_{out} 175,21 W, η 77,5%, P_{loss} 50,97 W.
 - Drive_Eff:** P_{in} 236,48 W, P_{out} 175,21 W, η 74,09%, P_{loss} 61,27 W.
- SCOPE of "System overview" (Bottom Left):** A waveform display showing current and voltage signals for Powersource.out.i, Inverter.out.L1, Inverter.out.L2, and Inverter.out.L3. The x-axis is time (11,100 s to 11,200 s) and the y-axis is current (A). A yellow ramp signal is also visible at the bottom.
- METER of "System overview" (Bottom Right):** A data table summarizing the system parameters.

Powersource.out			
P	236,42	u_{mean}	48,15
W		V	
i_{mean}	4,91	A	
A			
U	48,15	V	
V			
i_L	9,03	A	
A			
u_U	14,68	V	
V			
P_1	74,86	W	
W			
S_1	132,53	VA	
VA			
Q_1	109,37	var	
var			
λ_1	0,56		
i_L	9,03	A	
A			
u_U	14,68	V	
V			
P_1	74,86	W	
W			
S_1	132,53	VA	
VA			
Q_1	108,54	var	
var			
λ_1	0,57		
P_{mech}	175,26	n	1400,3
		M	1,12

Automatically Created ePower Suite Formulas

FOR Σ 44		START of Variable allocation	⊖
FOR Σ 45	Inverter.out.i_1	Recorder_A.Inverter.out.i_1	A
FOR Σ 46	Inverter.out.i_2	Recorder_A.Inverter.out.i_2	A
FOR Σ 47	Inverter.out.i_3	Recorder_A.Inverter.out.i_3	A
FOR Σ 48	Inverter.out.u_1	Recorder_A.Inverter.out.u_1	V
FOR Σ 49	Inverter.out.u_2	Recorder_A.Inverter.out.u_2	V
FOR Σ 50	Inverter.out.u_3	Recorder_A.Inverter.out.u_3	V



Allocation of measured phase quantities

FOR Σ 55		Defining cycle parameters	
FOR Σ 56	Inverter.out.Cycle_source	Recorder_A.Inverter.out.i_1	
FOR Σ 57	Inverter.out.Cycle_count	1	
FOR Σ 58	Inverter.out.Cycle_level	0	
FOR Σ 59	Inverter.out.Cycle_hyst_mode	1	
FOR Σ 60	Inverter.out.Cycle_hyst	5	
FOR Σ 61	Inverter.out.Cycle_holdoff	0.001	
FOR Σ 62	Inverter.out.Cycle_filter_type	1	
FOR Σ 63	Inverter.out.Cycle_cutoff_frequency	1000	
FOR Σ 64	Inverter.out.Cycle_direction	0	
FOR Σ 65	Inverter.out.Cycle_timeout	1	
FOR Σ 66	Inverter.out.Cycle_source_filt	@HWFilter (RTFormulas.Inverter.out.Cycle_source ; RTFormulas.Inverter.out.Cycle_filter_type ; RTFormulas.Inverter.out.Cycle_cul	
FOR Σ 67		End of cycle parameters	
FOR Σ 68		#endregion Cycle Parameters	
FOR Σ 69		=====	
FOR Σ 70		#region Cycle computation and Cycle check	
FOR Σ 71		START of Computing the CYCLE MASTER	
FOR Σ 72	Inverter.out.Cycle_Master	@CycleDetect (RTFormulas.Inverter.out.Cycle_source_filt ; RTFormulas.Inverter.out.Cycle_count ; RTFormulas.Inverter.out.Cycle_	



Cycle detection

Automatically Created ePower Suite Formulas

FOR Σ	101		As a first intermediate step the instantaneous power per phase is computed below	⊖
FOR Σ	102	Inverter.out.p_1	RTFomulas.Inverter.out.u_1 * RTFomulas.Inverter.out.i_1	W
FOR Σ	103	Inverter.out.p_2	RTFomulas.Inverter.out.u_2 * RTFomulas.Inverter.out.i_2	W
FOR Σ	104	Inverter.out.p_3	RTFomulas.Inverter.out.u_3 * RTFomulas.Inverter.out.i_3	W
FOR Σ	105		Then the total instantaneous power is the sum of the phase inst power // in [W]	⊖
FOR Σ	106	Inverter.out.p	RTFomulas.Inverter.out.p_1 + RTFomulas.Inverter.out.p_2 + RTFomulas.Inverter.out.p_3	W
FOR Σ	107		Then then mean over a cycle of each instantaneous power gives the active power below	⊖
FOR Σ	108	Inverter.out.P_1	@CycleMean (RTFomulas.Inverter.out.p_1 ; RTFomulas.Inverter.out.Cycle_Master)	W
FOR Σ	109	Inverter.out.P_2	@CycleMean (RTFomulas.Inverter.out.p_2 ; RTFomulas.Inverter.out.Cycle_Master)	W
FOR Σ	110	Inverter.out.P_3	@CycleMean (RTFomulas.Inverter.out.p_3 ; RTFomulas.Inverter.out.Cycle_Master)	W
FOR Σ	111		The sum of the active power per phase gives the total active power	⊖
FOR Σ	112	Inverter.out.P	RTFomulas.Inverter.out.P_1 + RTFomulas.Inverter.out.P_2 + RTFomulas.Inverter.out.P_3	W

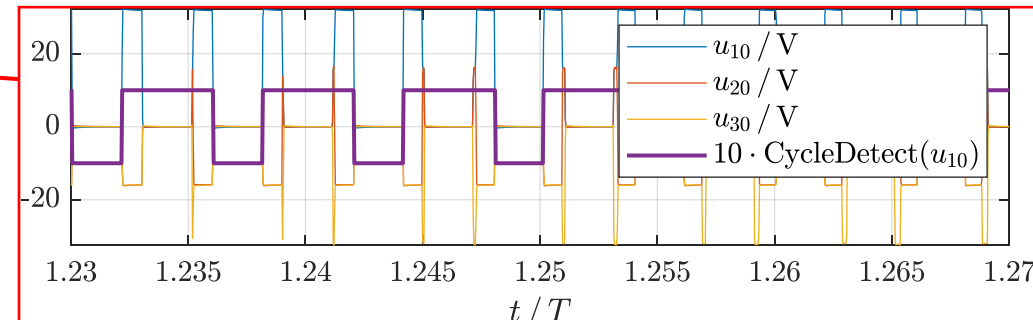
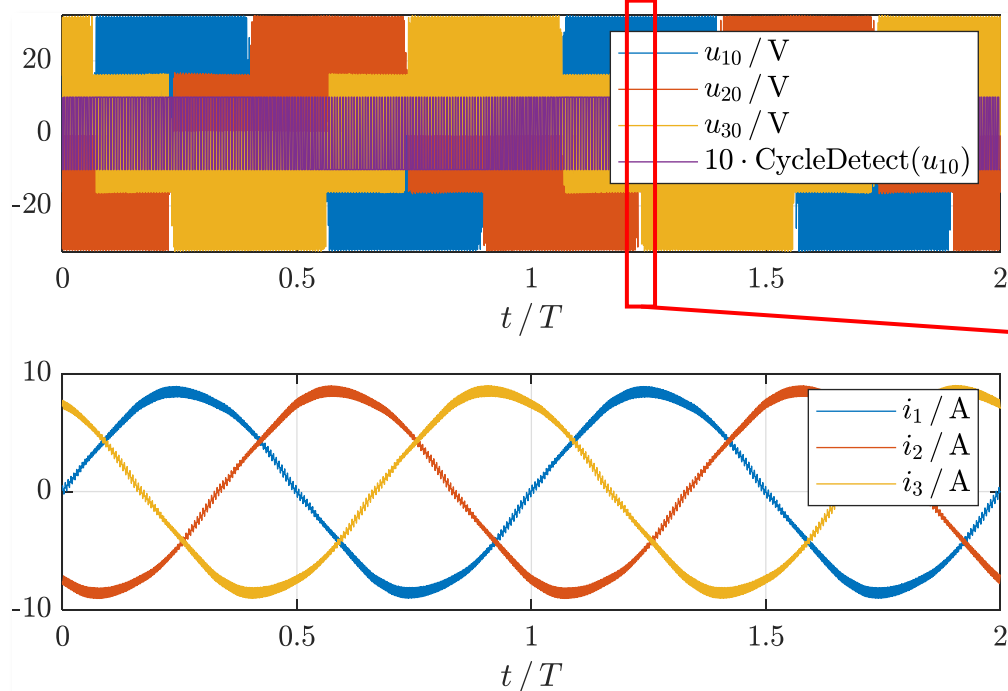
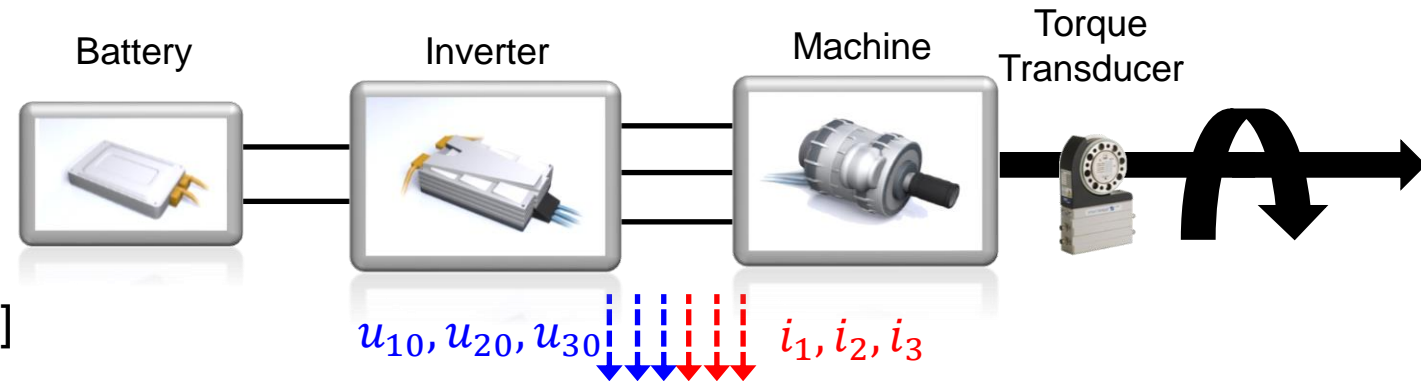


Power Calculation

Dynamic Electric Power Approximation

Input power of the machine

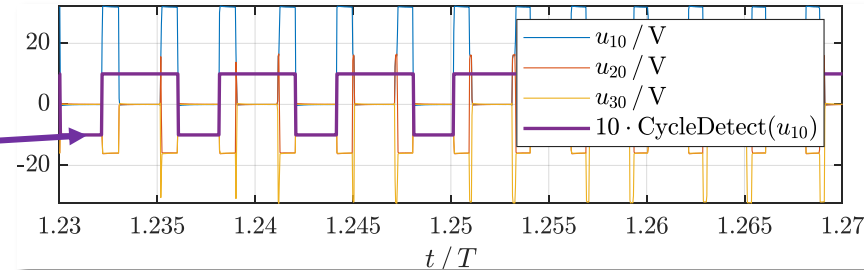
1. Measurement of the line currents and voltages
2. Detection of the switching cycle (based on pulsed voltage waveform) [6,9]



Dynamic Method to Estimate Electric Power

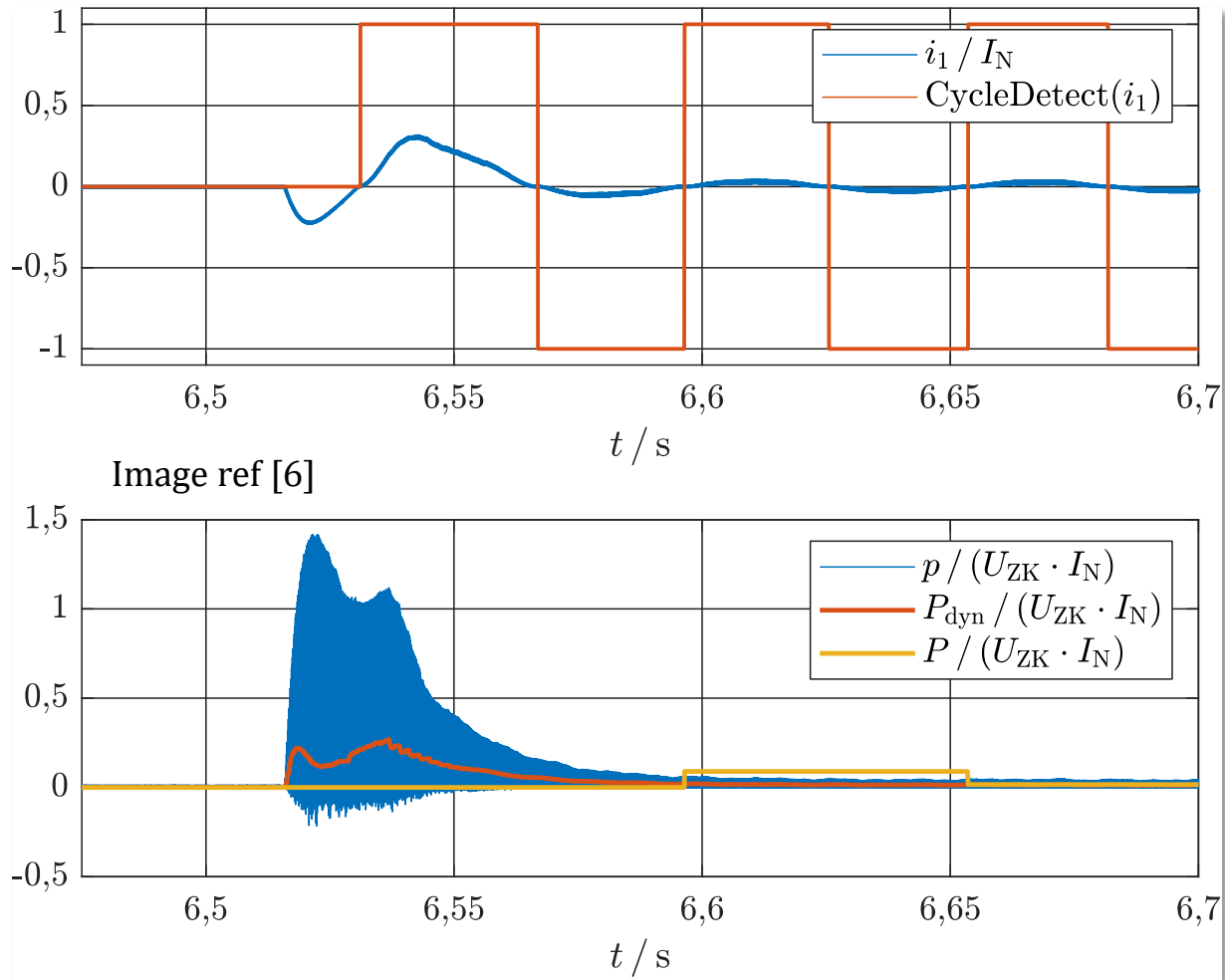
- Calculation of the **dynamic active power** as **average** of the instantaneous power related to the **switching period** T_s [6,9] → switching period is defined by the previously determined switching cycle

$$P_{\text{dyn}} = \overline{p(t)} \Big|_{T_s} = \frac{1}{T_s} \cdot \int_{T_s} p(\tau) d\tau$$



- This method is applicable for numerous PWM-methods
 - Provides an **approximation of the conventional active power** definition during **steady state**
 - Combines** the information of the **instantaneous power** $p(t)$ (during transients) and the **active power** P (during steady state) in a new dynamic active power definition P_{dyn}
 - The **quality of the approximation** becomes **better the larger T is compared to T_s** , i.e., $f_s > f$, resp.
 - It can be mathematically proven that the dynamic active power and the conventional definition of active power are analytically identical, see[6],...
 - ... in the theoretical ideal case of infinitely high switching frequency
 - ... certain restrictions are observed when generating the PWM

Comparative measurements – startup of a PMSM



→ Drastically increased dynamic and update rate of active power information

- ▲ No load acceleration from standstill to constant speed
- ▲ Due to causality, the first value of P can only be calculated after the first fundamental cycle is completed
 - at this point, the startup is already finished
- ▲ P_{dyn} is delayed only by one inverter switching cycle
 - provides a representative dynamic average of inst. power

Transition between different steady state operating points

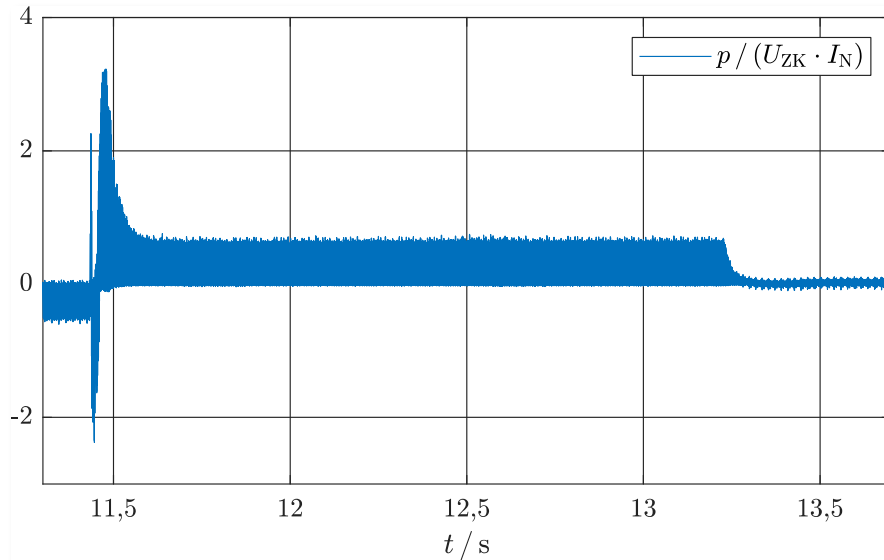
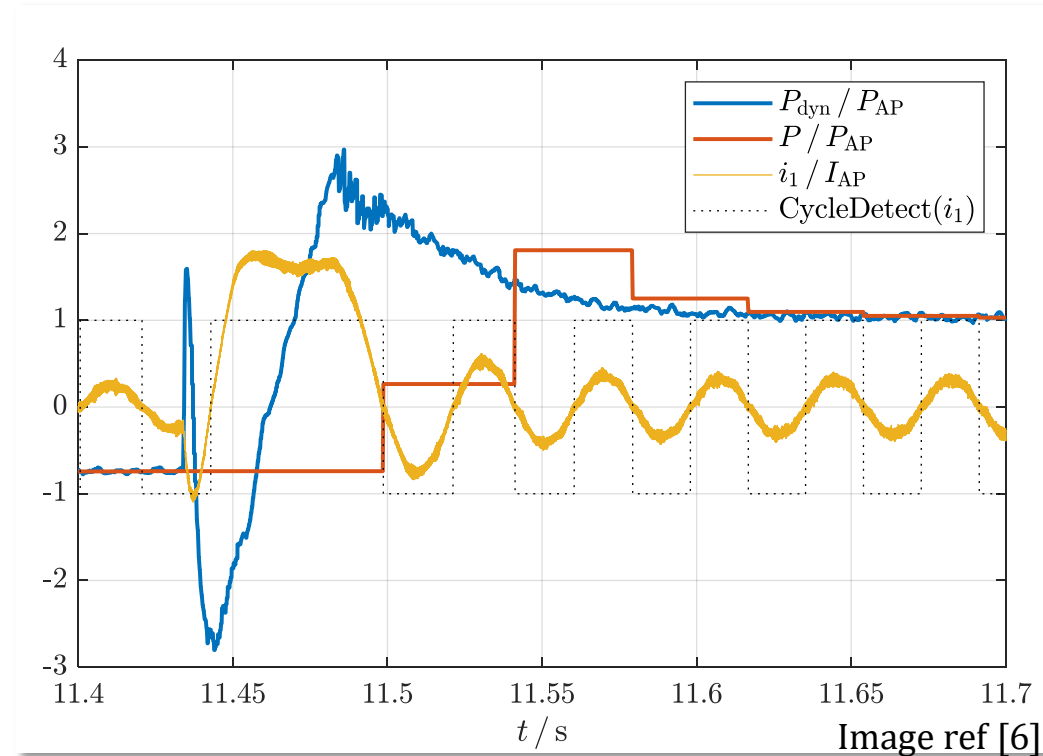
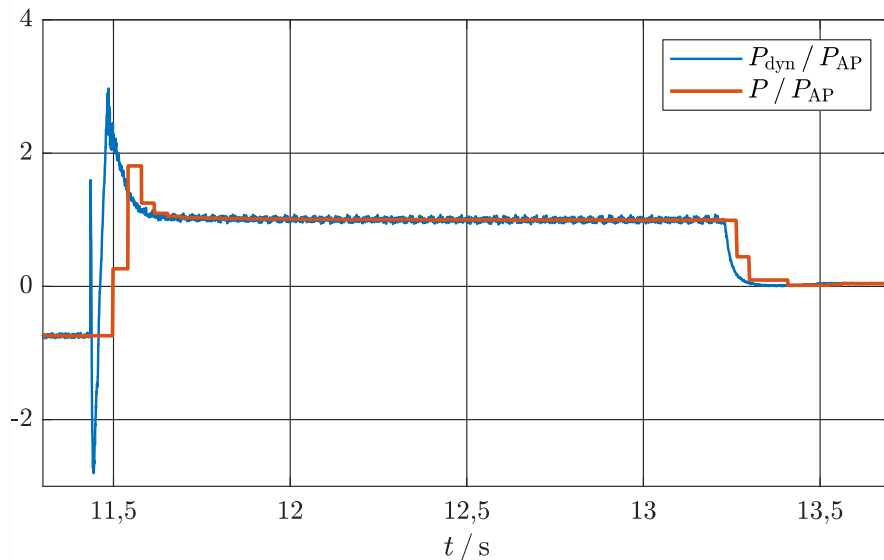
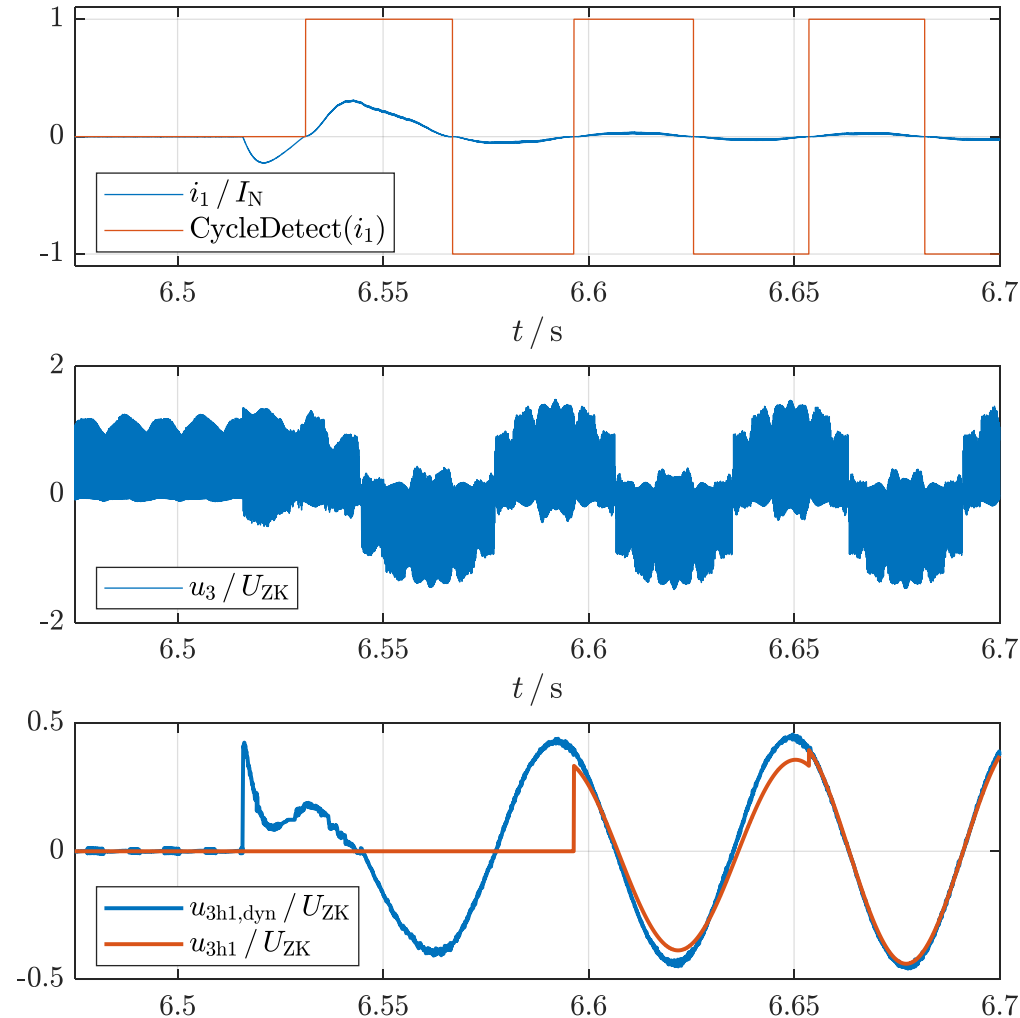


Image ref [6]



- ▲ P and P_{dyn} are very similar during steady state
- $f_s \approx 100 \cdot f$ for this measurement
- ▲ P_{dyn} provides significantly more dynamic information
- Precise active power approximation during steady state

Dynamic Fundamental Quantities



- Switching cycle-based averaging of the inverter output voltages, with $v \in \{1,2,3\}$

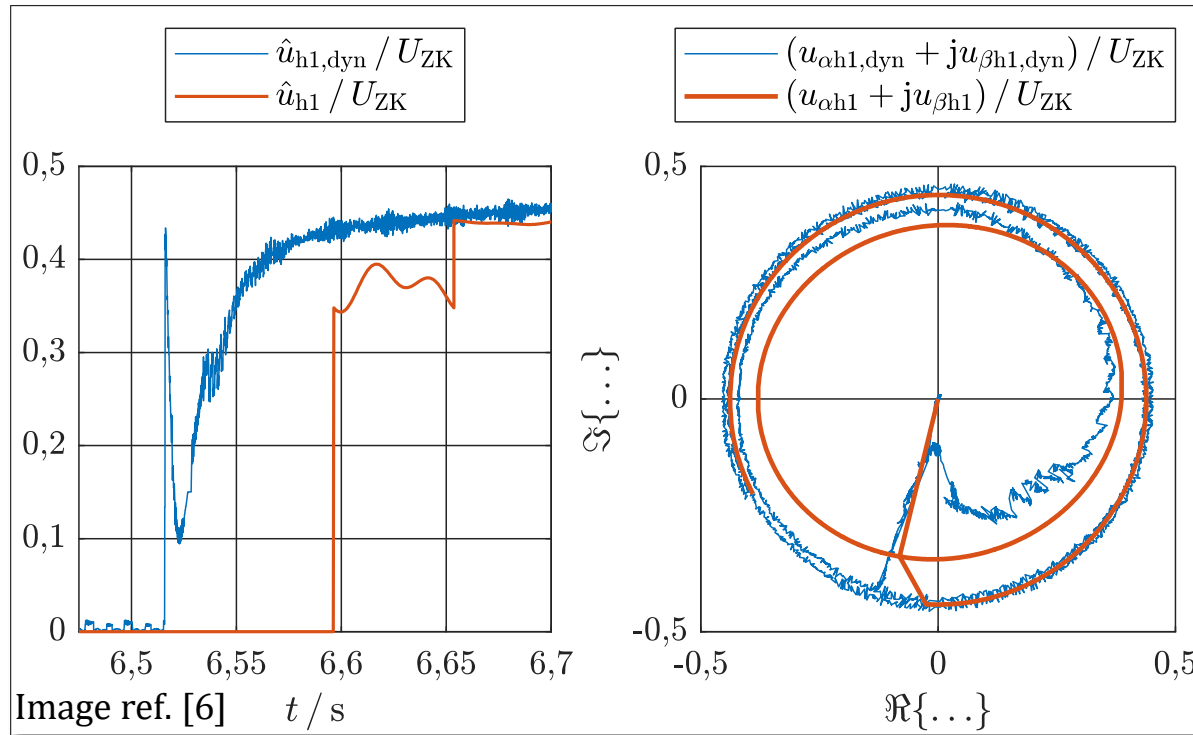
$$u_{vr,h1dyn} = \overline{u_{vr}(t)} \Big|_{T_s} = \frac{1}{T_s} \cdot \int_{T_s} u_{vr}(\tau) d\tau$$

- Subtraction of the zero-sequence voltage

$$u_{v,h1dyn} = u_{vr,h1dyn} - \sum_{\mu=1}^3 u_{vr,h1dyn}$$

→ Dynamic approximation of the fundamental waveforms

Fundamental Space Vectors



- Dynamic space vectors may be used to verify and assess the quality of the inverter control
- Fundamental dq0-Transform (Park-Transform) can be calculated

- ▶ Applying the space vector transformation (Clark-transformation) [4]

$$\begin{pmatrix} u_{\alpha h1,dyn} \\ u_{\beta h1,dyn} \end{pmatrix} = \begin{pmatrix} \frac{2}{3} & -\frac{1}{3} & -\frac{1}{3} \\ 0 & \frac{1}{\sqrt{3}} & -\frac{1}{\sqrt{3}} \end{pmatrix} \cdot \begin{pmatrix} u_{1h1,dyn} \\ u_{2h1,dyn} \\ u_{3h1,dyn} \end{pmatrix}$$

- ▶ Calculate the magnitude or phase angle of the space vector

$$\hat{u}_{h1,dyn} = \sqrt{u_{\alpha h1,dyn}^2 + u_{\beta h1,dyn}^2}$$

$$\varphi_{h1,dyn} = \text{atan2}(u_{\alpha h1,dyn}, u_{\beta h1,dyn})$$

Dynamic RMS Values

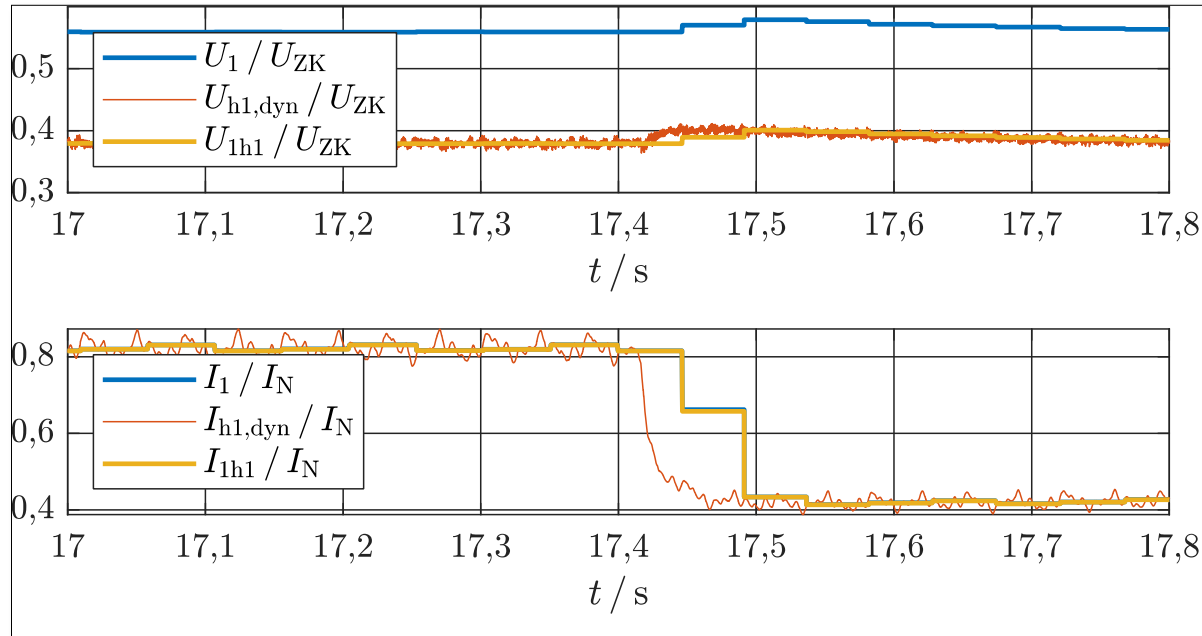


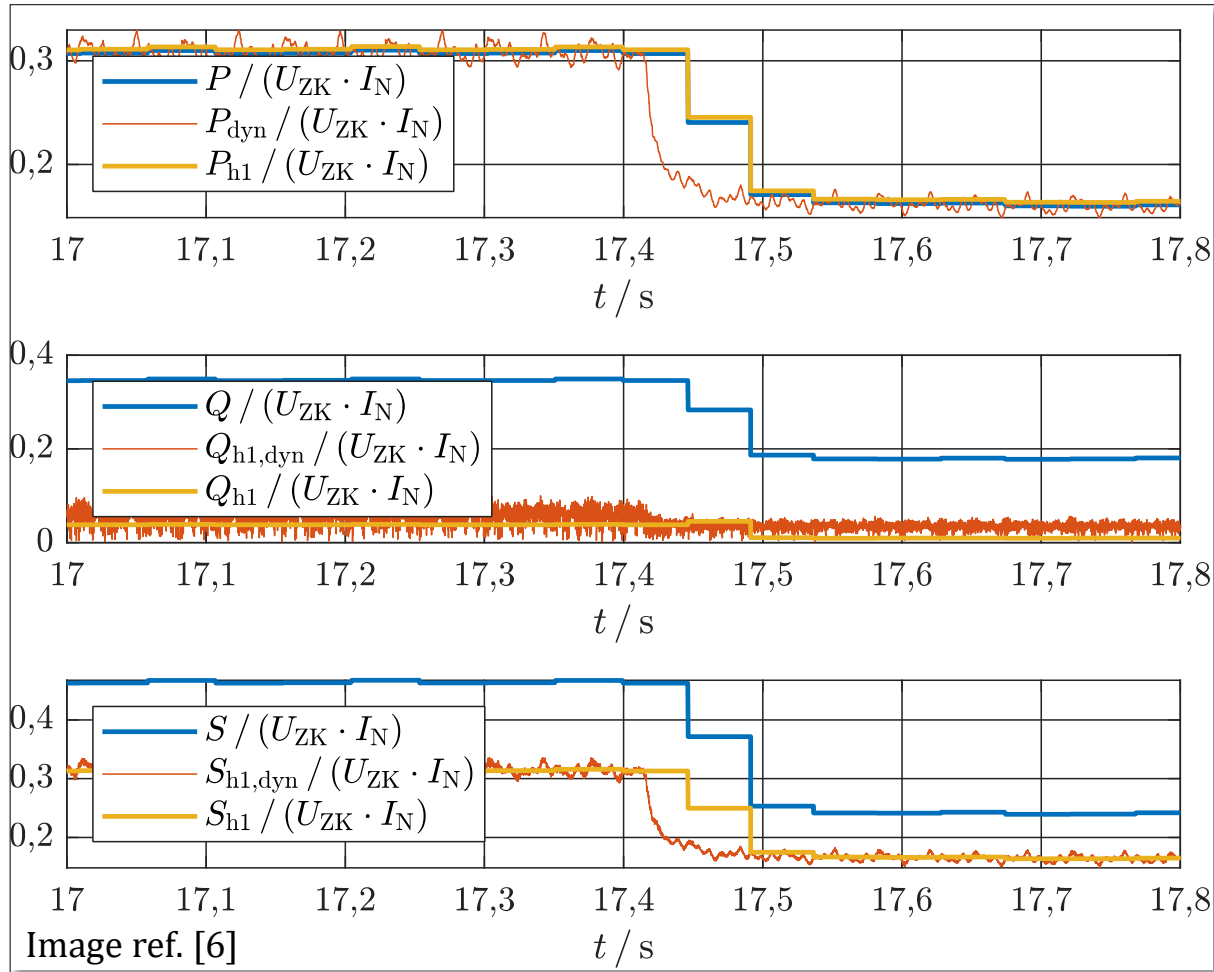
Image ref. [6]

- Assuming a balanced 3-phase system
 \rightarrow RMS values are calculated from the approximated fundamental space vector magnitude

$$U_{h1,dyn} = \frac{\hat{u}_{h1,dyn}}{\sqrt{2}}$$

- Same procedure for the current

Dynamic RMS Values & Power Quantities



- Dynamic (fundamental) active power

$$P_{\text{dyn}} = \overline{p(t)} \Big|_{T_s} = \frac{1}{T_s} \cdot \int_{T_s} p(\tau) d\tau$$

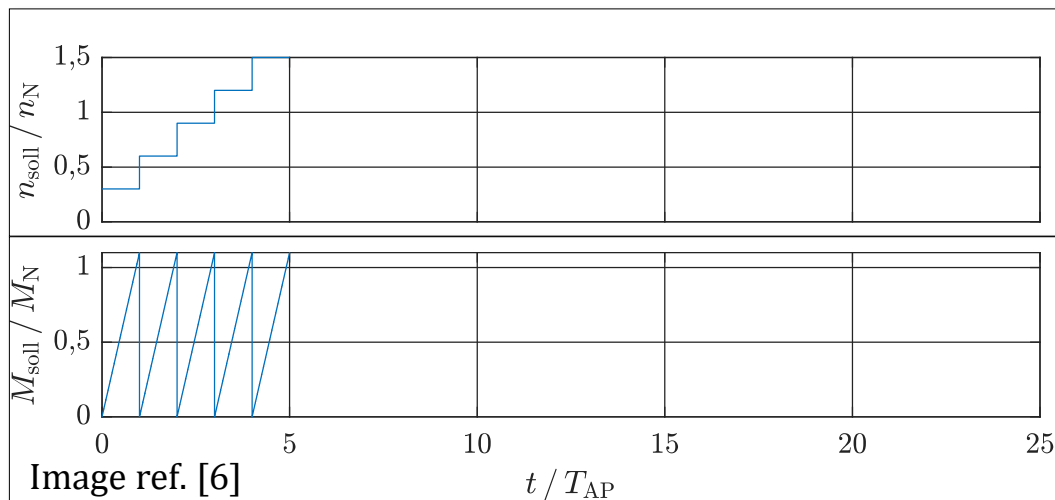
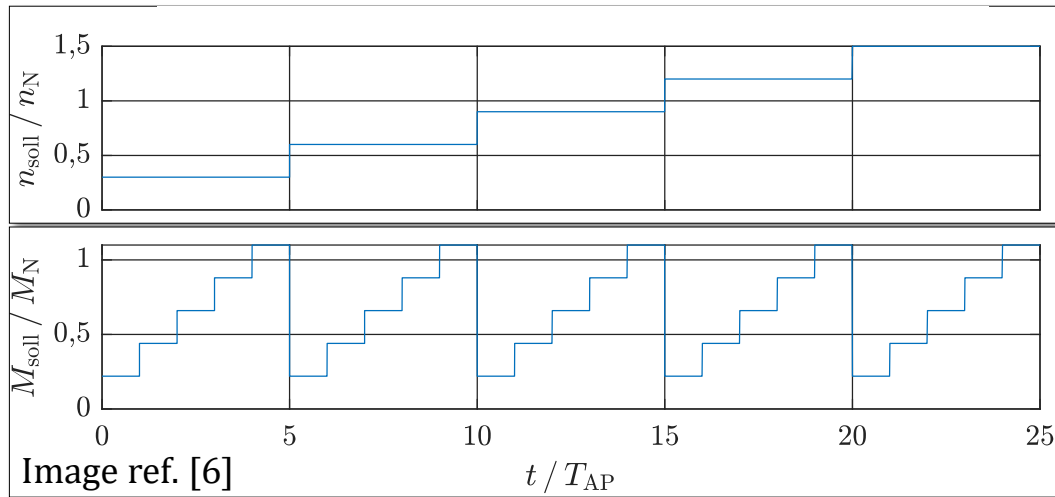
- Dynamic (fundamental) apparent power

$$S_{\text{h1,dyn}} = 3 \cdot U_{\text{h1,dyn}} \cdot I_{\text{h1,dyn}}$$

- Dynamic (fundamental) reactive power

$$Q_{\text{h1,dyn}} = \sqrt{S_{\text{h1,dyn}}^2 - P_{\text{dyn}}^2}$$

Accelerated Dynamic Efficiency Mapping



Conventional method

- Steady state set-point values of speed and torque are driven sequentially
- Conventional active power and mechanical power are calculated based on the fundamental cycle
- Efficiency is calculated

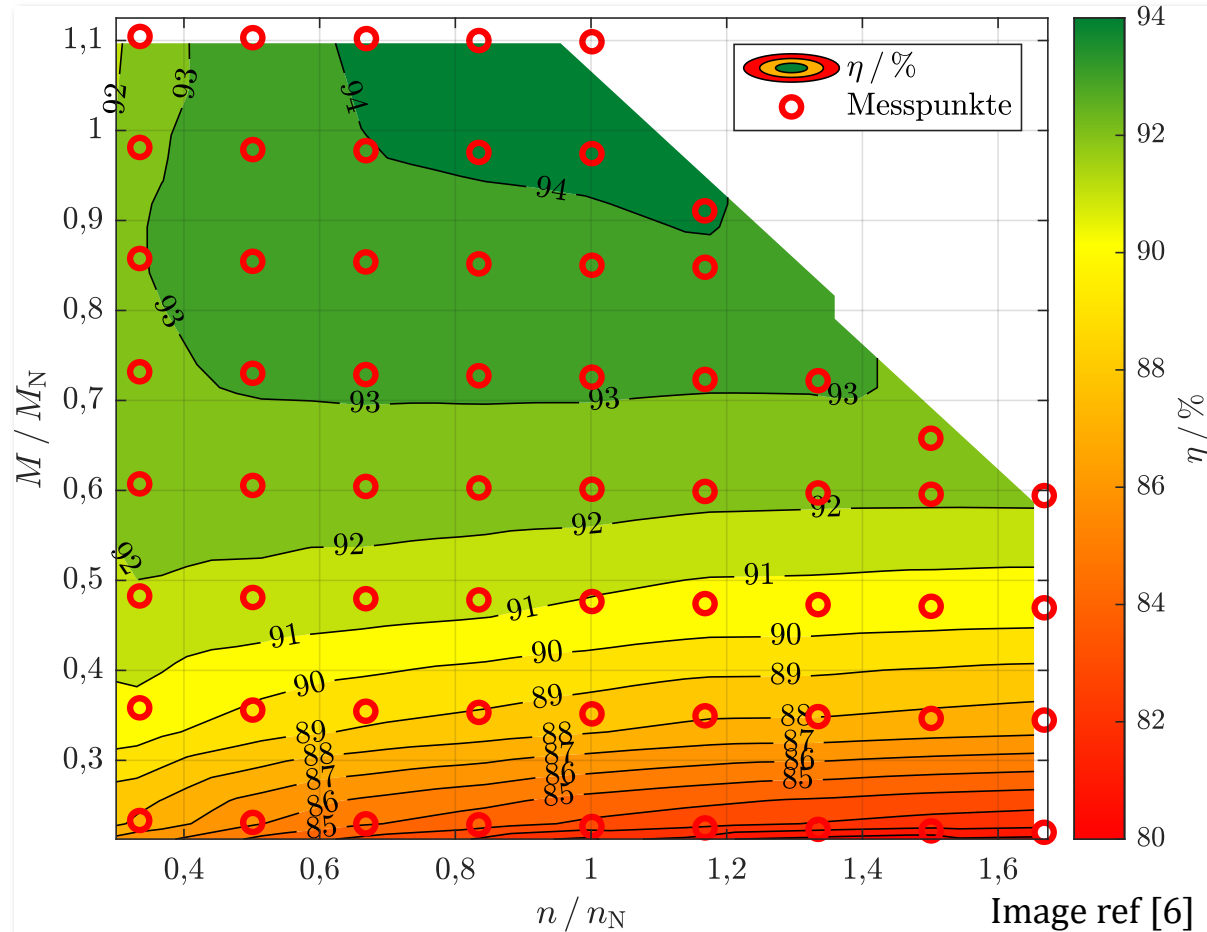
Dynamic method

- Steady state state set-point values of speed are driven sequentially
- For each speed, the torque is ramped up continuously
- Active power and mechanical power are calculated based on the inverter switching cycle

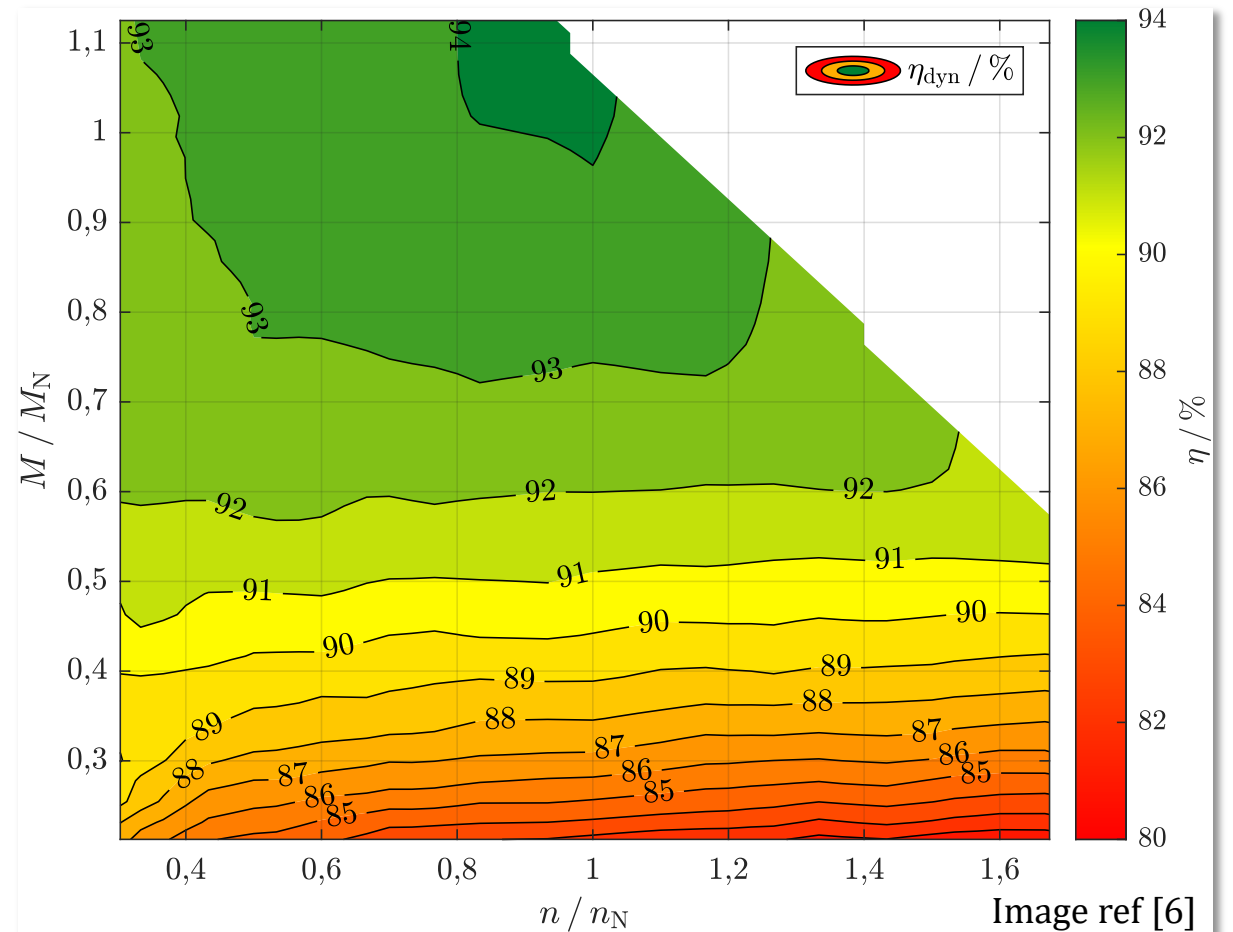
▲ **Significant time savings!**

Accelerated Dynamic Efficiency Diagram

Conventional Method



Dynamic Method



High level of similarity and enormously reduced measurement time

Accelerated Dynamic Efficiency Mapping

- Very small deviation between both methods
 - a small deviation from conventional method is inevitable
 - not suitable for the highest accuracy requirements, but:
- Accelerated measurement (time reduced to 10%)
 - Very suitable / cost efficient for end of line tests (pass/fail)
- Could also be evaluated during WLTP measurement
 - no additional efficiency measurement necessary

Deviation of Conventional and Dynamic Method

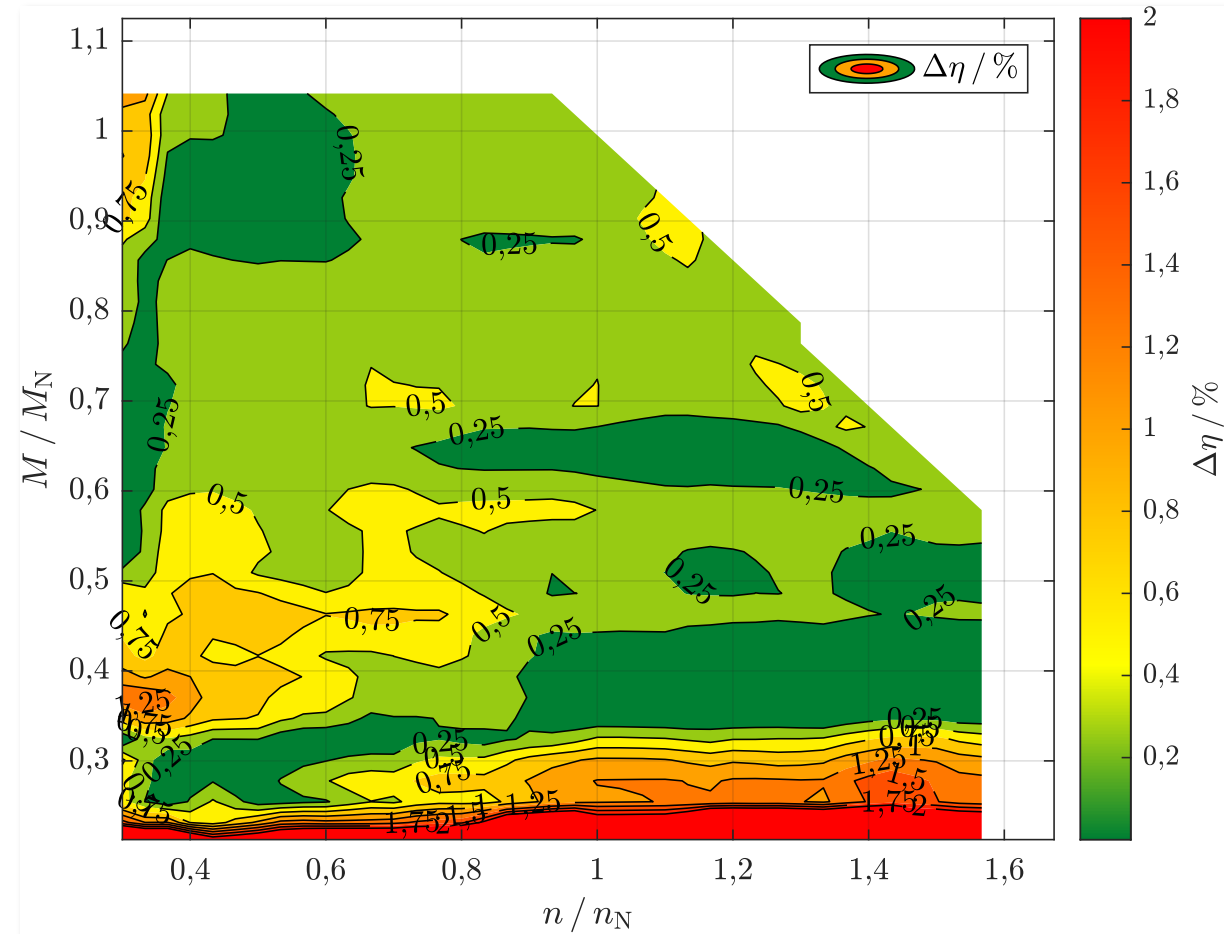


Image ref [6]

Summary

- ▲ Dynamic active power P_{dyn} was introduced as an additional new active power definition
- ▲ P_{dyn} combines the advantages of instantaneous power p and active power P in a new quantity
- ▲ Dynamic active power calculation method may be transferred to other cycle-based parameters, such as RMS, reactive power etc.
- ▲ P_{dyn} may be used to accelerated efficiency diagram measurements / save resources and costs
- ▲ Efficiency mapping may be included in test procedures to be done anyhow (e.g., WLTP tests)
- ▲ Suitable method for real-time measurements fed back into control algorithms (power control on the inverter system, double-two level inverter [7], doubly-fed PM synchronous machine [8])

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Bibliography

1. DIN 40110-1: Wechselstromgrößen Zweileiter-Stromkreise. 03/1994.
2. DIN 40110-2: Wechselstromgrößen Mehrleiter-Stromkreise. 11/2002.
3. IEEE Std 1459™-2010: IEEE Standard Definitions for the Measurement of Electric Power Quantities Under Sinusoidal, Nonsinusoidal, Balanced, or Unbalanced Conditions. 19. 03. 2010.
4. Teigelkötter, J.: *Energieeffiziente elektrische Antriebe. Grundlagen, Leistungselektronik, Betriebsverhalten und Regelung von Drehstrommotoren*. Wiesbaden: Springer-Vieweg, 2013.
5. Staudt, V.: „Fryze - Buchholz - Depenbrock: A time-domain power theory“. In: International School on Nonsinusoidal Currents and Compensation 2008 (Łagów, Polen). IEEE, 2008, S. 1-12.
6. Stock, A.: „*Messtechnische Analyse der Energieverluste von stromrichter gespeisten Antriebssystemen im nichtstationären Betrieb*“. Dissertation (submitted, not yet published). München: University of the German Federal Armed Forces, 2021.
7. Kowalski, T.: „*Mess- und Betriebsverfahren von stromrichter gespeisten Drehfeldmaschinen mit supraleitende Statorwicklung*“. Dissertation. Universität der Bundeswehr München, 2019.
8. Stock, A.; Teigelkötter, J.; Staudt, S.; Kowalski, T.: „*The Doubly Fed Permanent Magnet Synchronous Machine as a Highly Efficient Drive System for Constant Speed Applications*“. In: IEEE 11th International Conference on Power Electronics and Drive Systems (PEDS) (Sydney, Australia). IEEE, 2015.
9. Stock, A.; Teigelkötter, J.; Kowalski, T.; Staudt, S.; Ackermans, P.; Lang K.: „*Determination of active power on the basis of the switching frequency (Schaltfrequenzbasierte Wirkleistungsmessung)*“. Patent WO 2018/228655 A1. HBM Netherlands B.V. 20. 12. 2018.

Thank You

Questions?
Please don't hesitate to contact me...

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